

GeoMat Testing Laboratories, Inc.

Soil Engineering, Environmental Engineering, Materials Testing, Geology

March 14, 2016

Project No. 16027-02

TO: Mr. Shakil Patel, AIA
25982 Hinkley Street
Loma Linda, California 92354

SUBJECT: Basic Soil Infiltration Testing Report, Northwest Corner of Beaumont Avenue and Nevada Street, APN 029311150000, Redlands, California

Introduction

This report provides a summary of the geotechnical engineering services conducted to support evaluation of the feasibility of infiltration, in the upper five feet, at the subject site. The purpose of our services was to complete four insitu infiltration tests utilizing percolation testing procedure in boreholes to evaluate the feasibility of infiltration for disposal of stormwater runoff following the falling head method.

Scope of Services

GeoMat Testing Laboratories, Inc. was retained to provide geotechnical engineering services to support the project. Our scope of work consisted of the following specific tasks:

- 1) Drill three deep exploratory boreholes to maximum depth of 15 feet.
- 2) Complete four infiltration tests at the site utilizing the shallow boring percolation testing per San Bernardino County, Technical Guidance Document for Water Quality Management Plans procedures. The tests were completed in general accordance with the falling head method.
- 3) Complete laboratory gradation analysis and testing of selected soil sample.
- 4) Complete data analysis.
- 5) Preparation of this report summarizing our findings, conclusions, and recommendations. The report includes:
 - Site plan showing the location of infiltration tests.
 - Summary of site conditions observed at the testing locations.
 - Results of the laboratory testing.
 - Discussion of the results of insitu infiltration testing.
 - A discussion of the surficial soil and anticipated groundwater conditions at the site.
 - Evaluation of the feasibility of infiltration.
 - Recommendations for infiltration facility.

Existing Site Conditions

The subject site is located on the northwestern corner of Beaumont Avenue and Nevada Street, Redlands, California. Both Beaumont Avenue and Nevada Street are paved streets without curb or gutter. The geographical relationship of the site and surrounding vicinity is shown on our Site Location Map, Figure 1.

The site is approximately five and a half acres. Topography of the site is generally flat with a maximum relief of 9 feet. Surface drainage sheeting flows to the northwest at a rate of approximately 1.3%. Currently the site is vacant with light seasonal grasses sparsely spread about.

Groundwater

Groundwater study is not within the scope of this work. Groundwater was not encountered in our exploratory borings drilled at the site up to 15 feet below ground surface. Depth to groundwater is not expected to impact site grading.

Highest historical groundwater record documented by the State of California, Department of Water Resources in a well located approximately 1 mile northeast of the site (State Well No. 01S03W33C001S, elevation 1206) was 65 feet (water surface elevation of 1141) below ground surface on March 28, 1945. The lowest site elevation is approximately 1248 feet.

Please note that the potential for rain or irrigation water locally seeping through from elevated areas and showing up near grades cannot be precluded. Our experience indicates that surface or near-surface groundwater conditions can develop in areas where groundwater conditions did not exist prior to site development, especially in areas where a substantial increase in surface water infiltration results from landscape irrigation. Fluctuations in perched water elevations are likely to occur in the future due to variations in precipitation, temperature, consumptive uses, and other factors including mounding of perched water over bedrock. Mitigation for nuisance shallow seeps moving from elevated lower areas will be needed if encountered. These mitigations may include subdrains, horizontal drains, toe drains, french drains, heel drains or other devices.

Exploratory Boreholes

Three exploratory boreholes were drilled on February 28, 2016 to 15 feet below ground surface. The boreholes were drilled utilizing a CME 45 drill rig equipped with 8 inch hollow stem augers. The bottom of the exploratory borehole is estimated to be at least 10 feet below proposed bottom of infiltration facility.

Soil Sampling and Laboratory Testing

Bulk soil samples were obtained from the bottom of each percolation hole for laboratory classification. Laboratory sieve analysis was performed for the collected soil samples. The soil classifications are in conformance with the Unified Soil Classifications System (USCS), as outlined in the Classification and Symbols Chart (Appendix B).

A summary of our laboratory testing is presented in Appendix C. Based on laboratory testing the onsite soil is classified as silty sand with gravel and well graded sand with silt and gravel (USCS “SM”, “SPSM”).

Boring Percolation Testing Method

Four infiltration test holes were drilled with a mobile drill rig. A 4-inch-diameter perforated PVC casing wrapped with filter fabric was placed in the boreholes. Pea gravel was placed below and around the pipe for stability of the boreholes.

The boreholes were presoaked prior to the percolation testing. Presoaking was conducted using five gallon water bottles. All of soaking water seeped away while the technician is onsite.

After presoaking, infiltration boreholes were tested for and met the Sandy Soil Criteria. Infiltration testing continued for an additional hour with readings taken every ten minutes. The measurements were taken by filling up the test holes with water and allowing the water to percolate. The drop of water level was recorded every measurement. A stop watch was used to record the time measurements.

Infiltration Test Results

Four infiltration tests were conducted for the upper five feet of soil. Based on the results of this study, infiltration of stormwater at the site is feasible. The following summarizes the result of the infiltration feasibility study.

Test No.	Test Depth Below Ground Surface	Percolation Raw Rate (in/hr)	Adjusted Infiltration Rate (in/hr)
P-1	37"	35.3	3.7
P-2	44"	39.0	4.2
P-3	43"	30.0	3.1
P-4	42"	36.8	3.9

The percolation rate is the rate in horizontal and vertical direction. This rate is adjusted using Perchet Method for horizontal water infiltration. Refer to Appendix D for test results.

A safety factor should be applied to this rate by the design engineer. Safety factor discussion is in the following paragraph.

Factors of Safety

Long-term infiltration rates may be reduced significantly by factors such as soil variability and inaccuracy in the infiltration rate measurement. The correction factor for site variability is between 2 and 10. Safety factors for operating the system, maintenance, siltation, biofouling, etc. should also be considered by the design civil engineer at his discretion. Minimum safety factor for the infiltration rate required by the County of San Bernardino for tests conducted when deep exploratory borehole has been drilled at the site is at least 2.

Conclusions/Recommendations

- In our opinion, water infiltration at the site is feasible.
- Filter fabric should be used whenever aggregates are placed against native soils. Only washed aggregates are allowed.
- Infiltration water should not be allowed to saturate pavement and concrete structures subgrade soils.
- The test results may be utilized when the bottom of the infiltration system will be located within the alluvial soil observed/tested. Should this system be located in a different soil type, the infiltration characteristics will be different than those observed during the infiltration testing. The infiltration rate recommended above is based on the assumption that only clean water will be introduced to the subsurface profile. Any fines, debris, or organic materials could significantly impact the infiltration rate.
- Please note that soils in infiltration areas should not be subject to compaction during construction.
- The proposed system by the civil engineer should be constructed and maintained in accordance with manufacturer guidelines.

An important consideration for infiltration facilities is that, during construction, great care must be taken not to reduce the infiltrative capacity of the soil in the facility through compaction by heavy equipment or by using the infiltration area as a sediment trap.

Infiltration facilities should be located down gradient from structures and constructed late in the site development after soils (that might erode and clog the units) have been stabilized, or should be protected (by flagging) until site work is completed.

Infiltration facilities should be sited with the following guidelines:

INFILTRATION FACILITY SETBACKS	
Setback From	Distance
Property Lines and Public Right of Way	10 feet
Foundations/Slabs	15 feet or within a 1:1 plane drawn up from the bottom of foundation
Slopes	H/2, 5 feet minimum (H: is slope height)
Private drinking water wells	100 feet

Ferrous metal pipes should be protected from potential corrosion by bituminous coating, etc. We recommend that all utility pipes be nonmetallic and/or corrosion resistant. Recommendations should be verified by soluble sulfate and corrosion testing of soil samples obtained from specific locations during construction.

If applicable, rigid eight to twelve inch diameter, with locking cap, perforated observation well(s) extending vertically into the system's bottom is suggested as an observation point. Observation well(s) and associated appurtenances should be checked regularly throughout the year and after large storm event. Once performance stabilizes, frequency of monitoring may be reduced.

GeoMat Testing Laboratories should observe during facility excavation. Additional laboratory testing including but not limited to grain size analysis, sand equivalent, sulfate content, etc should be conducted during construction.

Use of this Report

This report was prepared for the exclusive use of the addressee and his consultants for specific application to the proposed site. The use by others, or for the purposes other than intended, is at the user's sole risk.

The findings, conclusions, and recommendations presented herein are based on our understanding of the project and on subsurface conditions observed during our site work. Within the limitations of scope, schedule, and budget, the conclusions and recommendations presented in this report were prepared in accordance with generally accepted geotechnical engineering principals and practices in the area at the time the report was prepared. We make no other warranty either expressed or implied.

We appreciate this opportunity to provide geotechnical services on this project and look forward to assisting the Project Team as the design progresses. If you have any questions or comments regarding the information contained in this report, or if we may be of further services, please call us at (951) 688-5400.

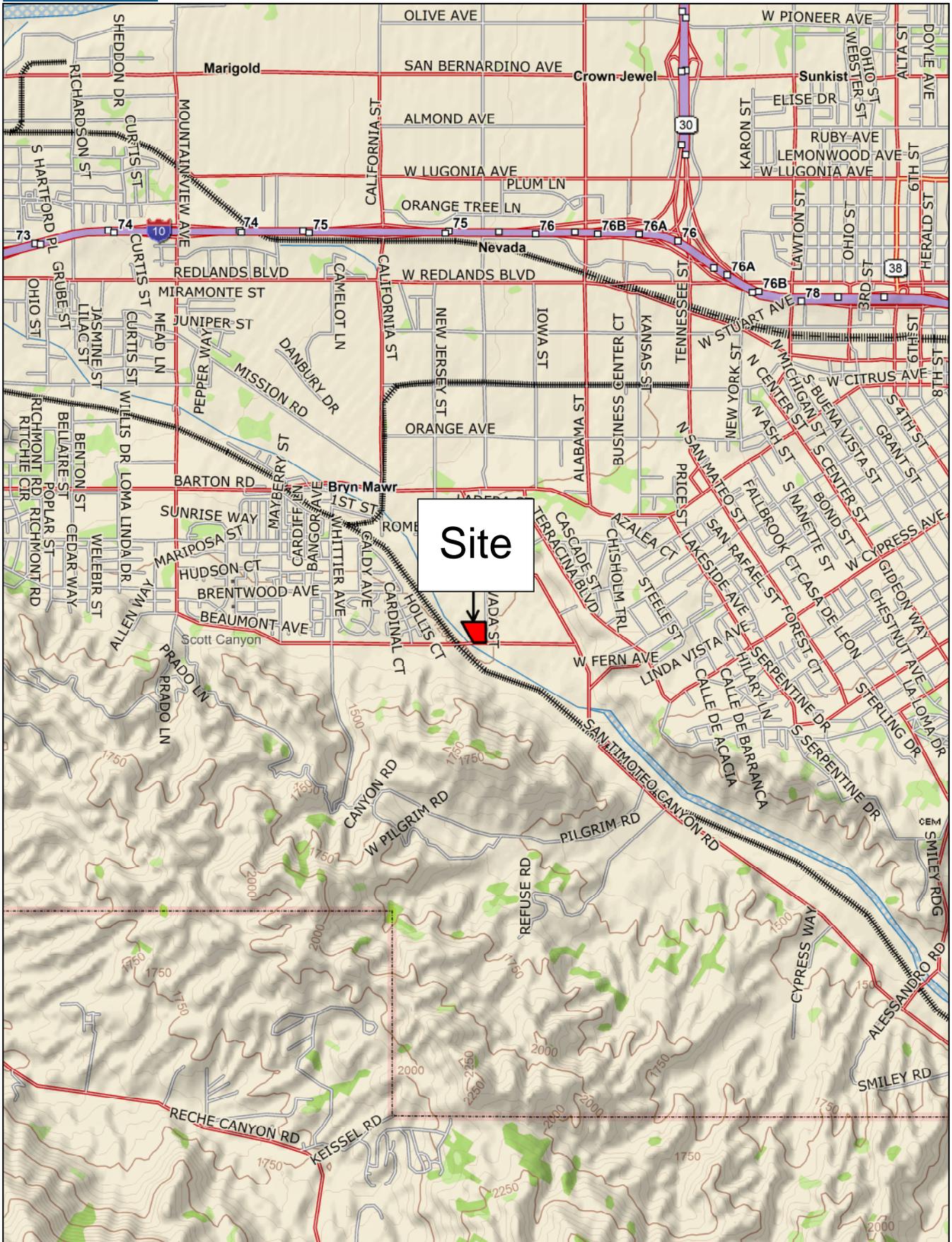
Submitted for GeoMat Testing Laboratories, Inc.

Haytham Nabilsli, GE 2375
Principal Engineer



Distribution: [3] Addressee

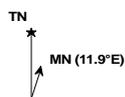
Attachments:	Figure 1	Site Location Map
	Plate 1	InfiltrationTest Location Map
	Appendix A	References
	Appendix B	Exploratory Borehole Logs
	Appendix C	Laboratory Test Results
	Appendix D	Infiltration Data/Graph



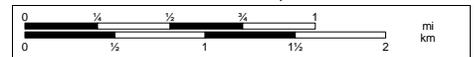
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Scale 1 : 50,000



1" = 4,166.7 ft

Data Zoom 12-0



DATE: 03/11/2016
 SHEET TITLE: SITE PLAN PHASE III
 PROJECT NO: 16027-01
 DRAWN BY: SP
 CHECKED BY: SP

APPLICANT: SHAHLI PATEL & ASSOCIATES AIA
 REDLANDS BLVD. LOYLA LINDA CA
 TEL: 951-746-6200
 patelshahli@gmail.com

ASSESSOR PARCEL NUMBER: APN 0242-152-3-4-0000
 ZONING: RL
 GENERAL PLAN LANDUSE: MULTI FAMILY RESIDENCE
 FRONT SETBACK: 25'-0"
 SIDE SETBACK: 25'-0"
 REAR SETBACK: 15'-0"

SITE DATA:
 LOT AREA: 5.50 AC
 BUILDING OCCUPANCY: AS BULLY UNPLANNED
 FIRST FLOOR: 9,500 SF

BUILDING DATA:
 LANDSCAPE AREA: 19,000 SF
 PAVING AREA: 10,150 SF
 LOT COVERAGE: 5.60 %
 PHASE II (NEXT 5 YEARS): 7,970 SF
 PHASE II (NEXT 10 YEARS): 6,800 SF
 TOTAL LOT COVERAGE REQUIRED: 28,600 SF @ 12 %
 MAXIMUM HEIGHT: 30 %

PARKING CALCULATION:
 REGULAR STALLS: 41-0'x18'-0" = 124 STALLS
 HANDICAPPED STALLS: 11'-0'x18'-0" = 6 STALLS
 ACCESSORY AREA: 12,000 SF / 1,000 SF = 12 STALLS
 REQUIRED STALLS: 142 STALLS

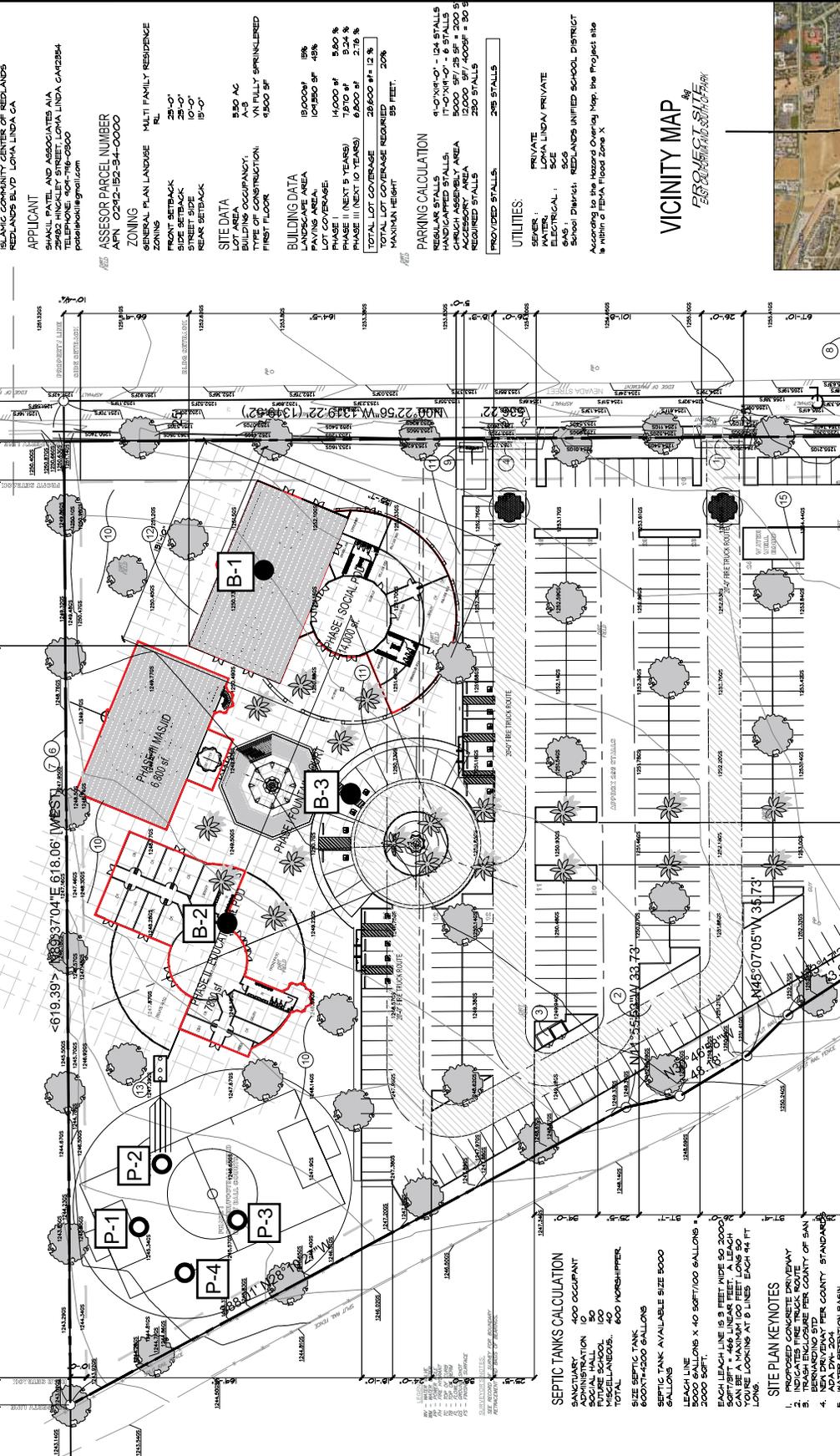
UTILITIES:
 PRIVATE: WATER, SEWER, GAS, ELECTRICAL, SLOPE
 PUBLIC: REDLANDS UNITED SCHOOL DISTRICT
 According to the Hazardous Overlay Map, the Project site is within a FEMA Flood Zone X.

VICINITY MAP
 PROJECT LOCATION

MASTER PLANNING PHASES

SITE PLAN PHASE III

A103



SEPTIC TANKS CALCULATION

BANQUET: 400 OCCUPANT
 ADMINISTRATION: 50
 SOCIAL HALL: 150
 MISCELLANEOUS: 500
 TOTAL: 600 MORPHIPPER

SIZE SEPTIC TANK: 600x1400 GALLONS
 SEPTIC TANK AVAILABLE SIZE: 5000 GALLONS

LEACH LINES: 4 x 40' x 50 FT/100 GALLONS = 2000 SQ FT
 EACH LEACH LINE IS 8 FEET WIDE 50 SQ FT/8 FT = 400 LINEAR FEET. A LEACH CAN BE A MAXIMUM 100 FEET LONG 50' LONG. LOOKING AT 8 LINES, EACH 44 FT LONG.

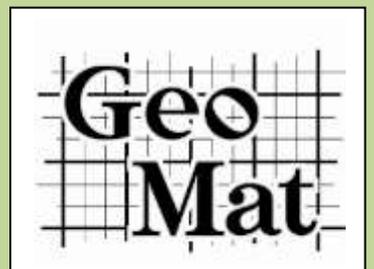
SITE PLAN KEY/NOTES

- INDICATED FIRE TRUCK ROUTE
- TRASH ENCLOSURE PER COUNTY OF SAN DIEGO
- NEW DRIVEWAY PER COUNTY STANDARDS
- ADDITIONAL 204
- ADDITIONAL 204

GeoMat Testing Laboratories, Inc.
 Exploratory Borehole/Percolation Test Map
 Project No. 16027-01
 Plate 1
 March 11, 2016

- Approximate Location of Exploratory Borehole
- Approximate Location of Percolation/Infiltration Tests

Appendix A



REFERENCES

Shakil Patel & Associates' Islamic Community Center of Redlands, Northwest Corner of Beaumont Avenue and Nevada Street, Redlands, California, Site Plan Phase III, Sheet A103, Plan Dated February 2, 2016.

Technical Guidance Document for Water Quality Management Plans, The County of San Bernardino Areawide Stormwater Program, NPDES No. CAS618036, Order No. R8-2010-0036.

San Bernardino County Stormwater Program, Model Water Quality Management Plan Guidance, Jun. 9, 2005.

Riverside County, Stormwater Quality Best Management Practice, Design Handbook, July 21, 2006

Riverside County, Design handbook for Low Impact Development Best management Practices, September 2011.

Riverside County, Water Quality Management Plan For Urban Runoff, Santa Ana River Region, Santa Margarita River Region, September 17, 2004

California Stormwater Quality Association, Stormwater Best Management Practice, Handbook, Jan. 2003.

California Department of Transportation, Stormwater Quality Handbook, Project Training and Design Guide, Sacramento, 2000.

California Department of Transportation, Stormwater Quality Handbook, Project Planning and Design Guide, Sacramento, 2005.

Federal Highway Administration, Urban Design Drainage Manual, Washington DC, 1996

Massmann, JW, Butchart, and S Stolar, Infiltration Characteristics, Performance, and Design of Stormwater Facilities, Final Research Report, Research Project TI 803, Task 12, Washington DOT 2003.

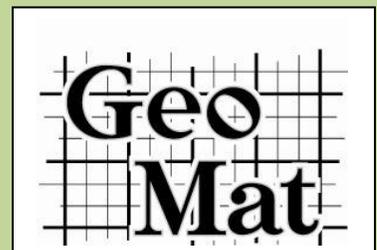
Soilvision Systems, A Knowledge-Based Soils Database, Murray Fredlund, Canada, 2004.

US Environmental Protection Agency, Storm water Technology Fact Sheet, Infiltration Trench, EPA 832-F-99-019, 1999.

California Stormwater Quality Association (QASCA), California Stormwater BMP Handbook, Infiltration Trench, TC-10 Design Considerations

BMP Handbook, Part B, Planning Activities, Stormwater Mitigation Measures, Watershed Protection Division, City of Los Angeles.

Appendix B



WATER LEVEL MEASUREMENTS

Water levels indicated on the boring logs are levels measured in the borings at the times indicated. In permeable materials, the indicated levels may reflect the location of groundwater. In low permeability soils, the accurate determination of groundwater levels is not possible with only short-term observations.

WATER LEVEL OBSERVATION DESIGNATION

W.D.	While Drilling
A.B.	After Boring
B.C.R.	Before Casing Removal
A.C.R.	After Casing Removal
24 hr.	Water level taken approximately 24 hrs. after boring completion

DRILLING AND SAMPLING SYMBOLS

AS	Auger Sample
CS	Continuous Sampler
DB	Diamond Bit -NX unless otherwise noted
HA	Hand Auger
HS	Hollow Stem Auger
PA	Power Auger
RB	Rock Bit
SS*	Split-Barrel
ST	Shelby Tube - 2" (51mm) unless otherwise noted
WB	Wash Bore
CR	California Ring Sampler 3" O.D., Lined with 2.5"X1" Rings

*The Standard Penetration Test is conducted in conjunction with the split-barrel sampling procedure. The "N" value corresponds to the number of blows required to drive the last 1 foot (0.3m) of an 18 in. (0.46m) long, 2 in. (51mm) O.D. split-barrel sampler with a 140 lb. (63.5 kg) hammer falling a distance of 30 in. (0.76m). The Standard Penetration Test is carried out according to ASTM D-1586. (See "N" Value below.)

SOIL PROPERTIES & DESCRIPTIONS

TEXTURE

PARTICLE	SIZE
Clay	< 0.002 mm (< 0.002 mm)
Silt	< #200 Sieve (0.075 mm)
Sand	#4 to #200 Sieve (4.75 to 0.075 mm)
Gravel	3 in. to #4 Sieve (75 mm to 4.75 mm)
Cobbles	12 in. to 3 in. (300 mm to 75 mm)
Boulders	> 12 in. (300 mm)

COMPOSITION

SAND & GRAVEL	
Description	% by Dry Weight
trace	< 15
with modifier	15 - 29
	> 30
FINES	
Description	% by Dry Weight
trace	< 5
with modifier	5 - 12
	> 12

Soil descriptions are based on the Unified Soil Classification System (USCS) as outlined in ASTM Designations D-2487 and D-2488. The USCS group symbol shown on the boring logs correspond to the group names listed below. The description includes soil constituents, consistency, relative density, color and other appropriate descriptive terms. Geologic description of bedrock, when encountered, also is shown in the description column.

GROUP SYMBOL	GROUP NAME	GROUP SYMBOL	GROUP NAME
GW	Well Graded Gravel	CL	Lean Clay
GP	Poorly Graded Gravel	ML	Silt
GM	Silty Gravel	OL	Organic Clay or Silt
GC	Clayey Gravel	CH	Fat Clay
SW	Well Graded Sand	MH	Elastic Silt
SP	Poorly Graded Sand	OH	Organic Clay or Silt
SM	Silty Sand	PT	Peat
SC	Clayey Sand	CL-CH	Lean to Fat Clay

COHESIVE SOILS

CONSISTENCY	UNCONFINED COMPRESSIVE STRENGTH (Qu) (psf)	COMPRESSIVE STRENGTH (kPa)	PLASTICITY
Very Soft	< 500	(< 24)	Description
Soft	500 - 1000	(24 - 48)	Lean
Medium	1001 - 2000	(48 - 96)	Lean to Fat
Stiff	2001 - 4000	(96 - 192)	Fat
Very Stiff	4001 - 8000	(192 - 383)	
Hard	> 8001	(> 383)	

Cohesive Soils	
Consistency	"N" value
Very Soft	<2
Soft	2-4
Medium	4-8
Stiff (Firm)	8-15
Very Stiff (Very Firm)	15-30
Hard	>30

COHESIONLESS SOILS

RELATIVE DENSITY	"N" VALUE*
Very Loose	0 - 3
Loose	4 - 9
Medium Dense	10 - 29
Dense	30 - 49
Very Dense	≥ 50

BEDROCK PROPERTIES & DESCRIPTIONS

ROCK QUALITY DESIGNATION (RQD**)

DESCRIPTION OF ROCK QUALITY	RQD (%)
Very Poor	0 - 25
Poor	25 - 50
Fair	50 - 75
Good	75 - 90
Excellent	90 - 100

**RQD is defined as the total length of sound core pieces, 4 inches (102mm) or greater in length, expressed as a percentage of the total length cored. RQD provides an indication of the integrity of the rock mass and relative extent of seams and bedding planes.

DEGREE OF WEATHERING

Slightly Weathered	Slight decomposition of parent material in joints and seams.
Weathered	Well-developed and decomposed joints and seams.
Highly Weathered	Rock highly decomposed, may be extremely broken.

SOLUTION AND VOID CONDITIONS

Solid	Contains no voids.
Vuggy	Containing small pits or cavities < 1/2" (13mm).
Porous	Containing numerous voids which may be interconnected.
Cavernous	Containing cavities, sometimes quite large.

When classification of rock materials has been estimated from disturbed samples, core samples and petrographic analysis may reveal other rock types.

HARDNESS & DEGREE OF CEMENTATION

LIMESTONE	
Hard	Difficult to scratch with knife.
Moderately Hard	Can scratch with knife but not with fingernail.
Soft	Can be scratched with fingernail.
SHALE	
Hard	Can scratch with knife but not with fingernail.
Moderately Hard	Can be scratched with fingernail.
Soft	Can be molded easily with fingers.
SANDSTONE	
Well Cemented	Capable of scratching a knife blade.
Cemented	Can be scratched with knife.
Poorly Cemented	Can be broken apart easily with fingers.

BEDDING CHARACTERISTICS

TERM	THICKNESS (inches)	THICKNESS (mm)
Very Thick Bedded	> 36	> 915
Thick Bedded	12 - 36	305 - 915
Medium Bedded	4 - 12	102 - 305
Thin Bedded	1 - 4	25 - 102
Very Thin Bedded	0.4 - 1	10 - 25
Laminated	0.1 - 0.4	2.5 - 10
Thinly Laminated	< 0.1	< 2.5
Bedding Planes	Planes dividing the individual layers, beds or strata of rocks.	
Joint	Fracture in rock, generally more or less vertical or transverse to the bedding.	
Seam	Applies to bedding plane with an unspecified degree of weathering.	

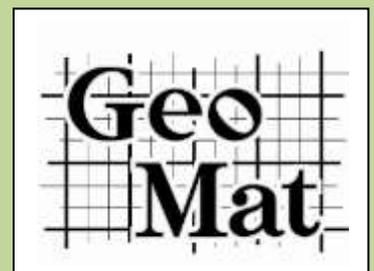
BORHOLE LOG				BH-1		Sheet		1	OF	1								
Project No.				16027-01		Date		2/28/2016										
Project				Redlands Masjid		Drilling Rig		CME 45										
Client				Mr. Shakil Patel		Sampler		Cal Mod. And SPT										
Location				APN 0293-111-15-0000, Redlands, CA		Method		Hollow Stem										
Coordinate						Hammer Type		140 lb										
Notes						Surface Elev.												
						Total Depth		15'										
Type/Symbol	Casing	Split Spoon	Ring Sampler	Cutting	Date	Time	Water Depth (ft)	Casing Size (in)	Casing Depth (ft)	Moisture (%)	Dry Density (pcf)	Symbol						
I.D.		S	R	C	2/28/2016		None											
O.D.																		
Length																		
Hammer Wt.																		
Hammer Fall																		
Depth Below Surface (ft)	Elevation (ft)	Soil Sample				Blows				VISUAL MATERIAL CLASSIFICATION AND REMARKS			Moisture (%)	Dry Density (pcf)	Test			
		Type	Number	Symbol	Depth	0-152.4 mm	152.4-304.8 mm	304.8-457.2 mm	N-Value							N60	(N1)60	
0																		
1																		
2																		
3		R		⚡	10	13	15	18					2	121				
4																		
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The stratification lines represent the approximate boundary lines between soil and rock types. In-situ, the transition may be gradual.

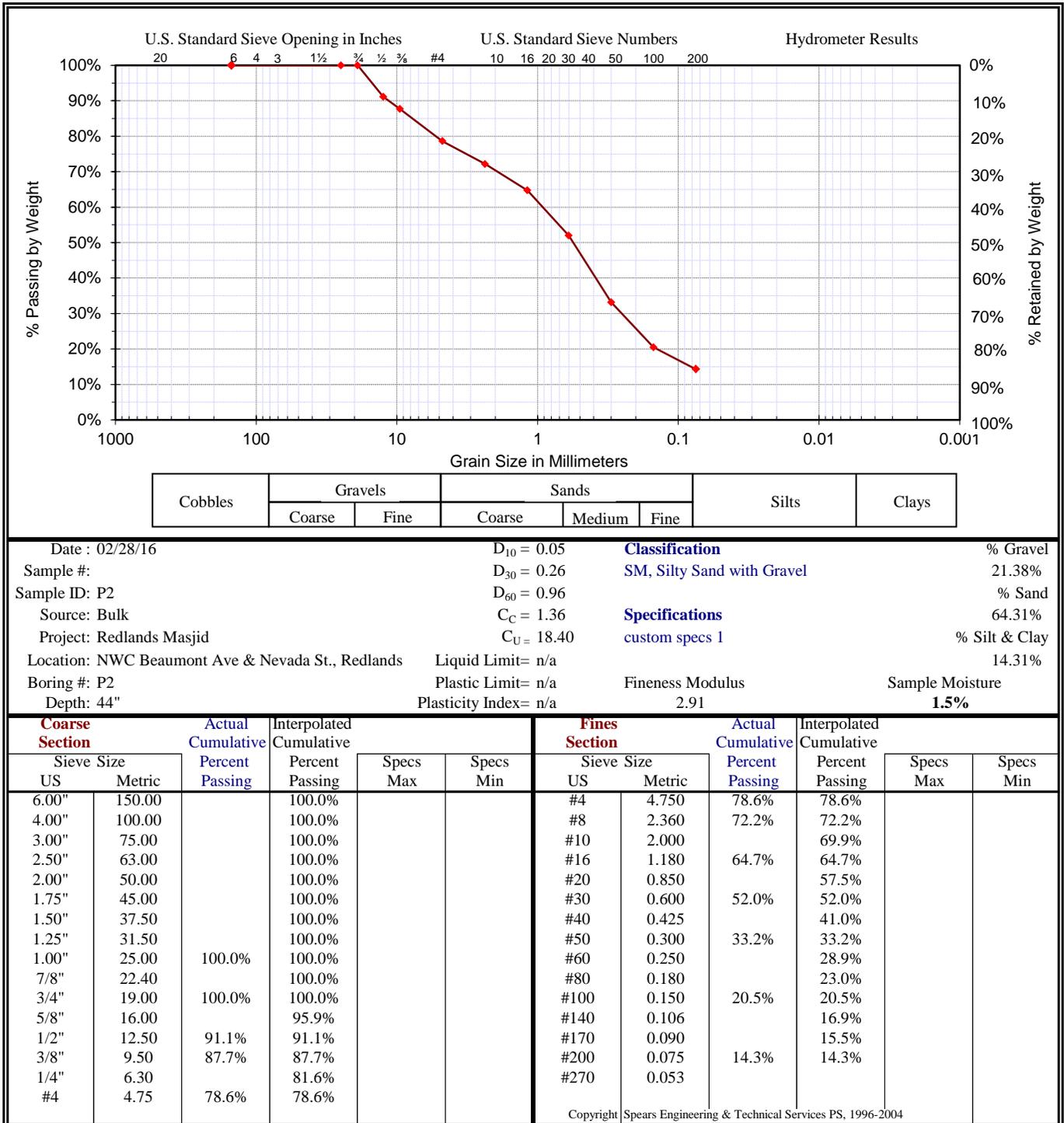
BORHOLE LOG				BH-3		Sheet		1	OF	1									
Project No.				16027-01		Date		2/28/2016											
Project				Redlands Masjid		Drilling Rig		CME 45											
Client				Mr. Shakil Patel		Sampler		Cal Mod. And SPT											
Location				APN 0293-111-15-0000, Redlands, CA		Method		Hollow Stem											
Coordinate						Hammer Type		140 lb											
Notes						Surface Elev.													
						Total Depth		15'											
Type/Symbol	Casing	Split Spoon	Ring Sampler	Cutting	Date	Time	Water Depth (ft)	Casing Size (in)	Casing Depth (ft)	Hole Depth (ft)	Symbol								
I.D.		S	R	C	2/28/2016		None												
O.D.																			
Length																			
Hammer Wt.																			
Hammer Fall																			
Depth Below Surface (ft)	Elevation (ft)	Soil Sample			Blows			VISUAL MATERIAL CLASSIFICATION AND REMARKS				Moisture (%)	Dry Density (pcf)	Test					
		Type	Number	Symbol	Depth	0-152.4 mm	152.4-304.8 mm								304.8-457.2 mm	N-Value	N60	(N1)60	
0																			
1																			
2																			
3																			
4																			
5		R		▲	10	19	33	34					6	121					
6																			
7																			
8																			
9																			
10		S		■	13	17	18	35											
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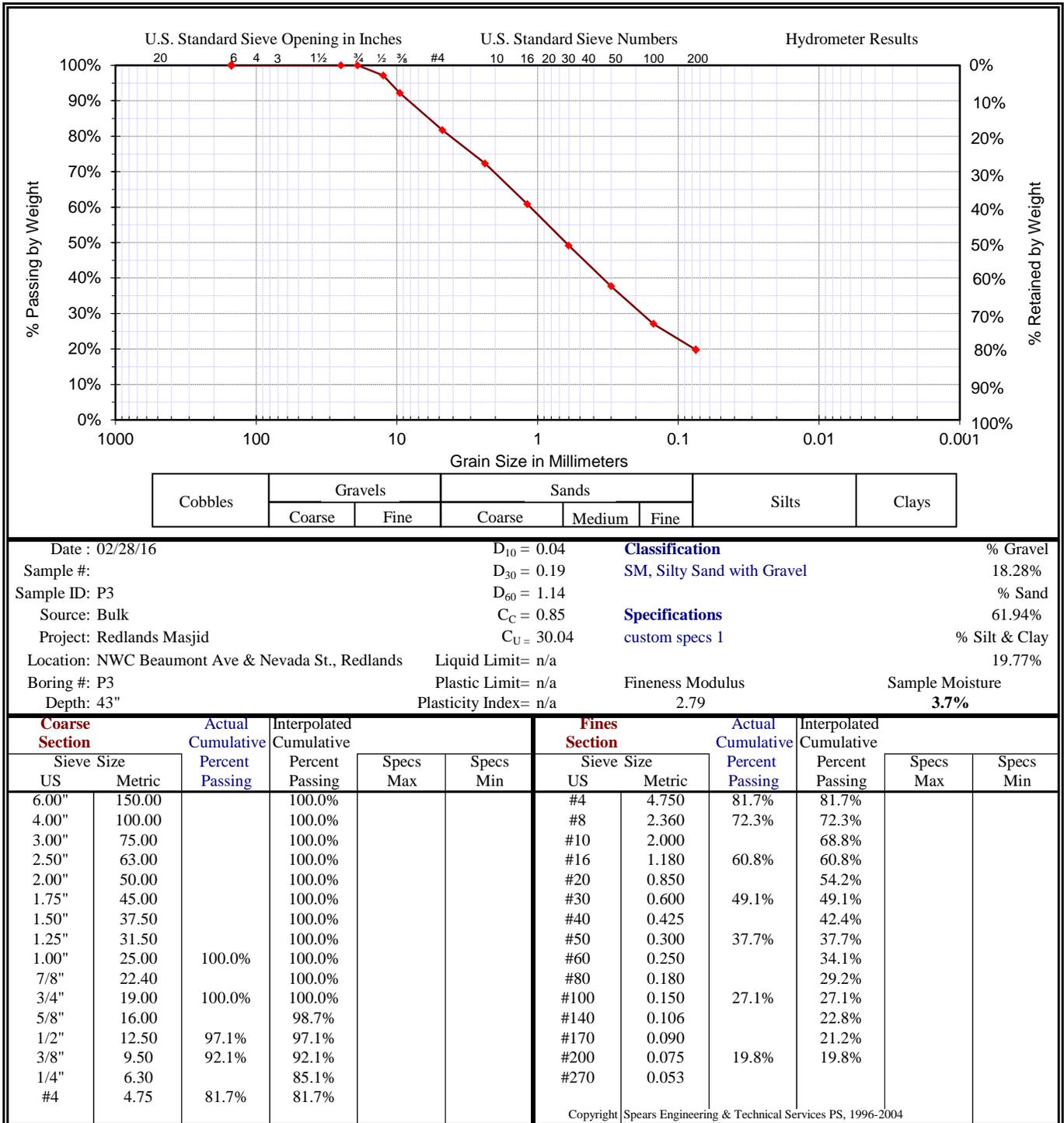
Appendix C



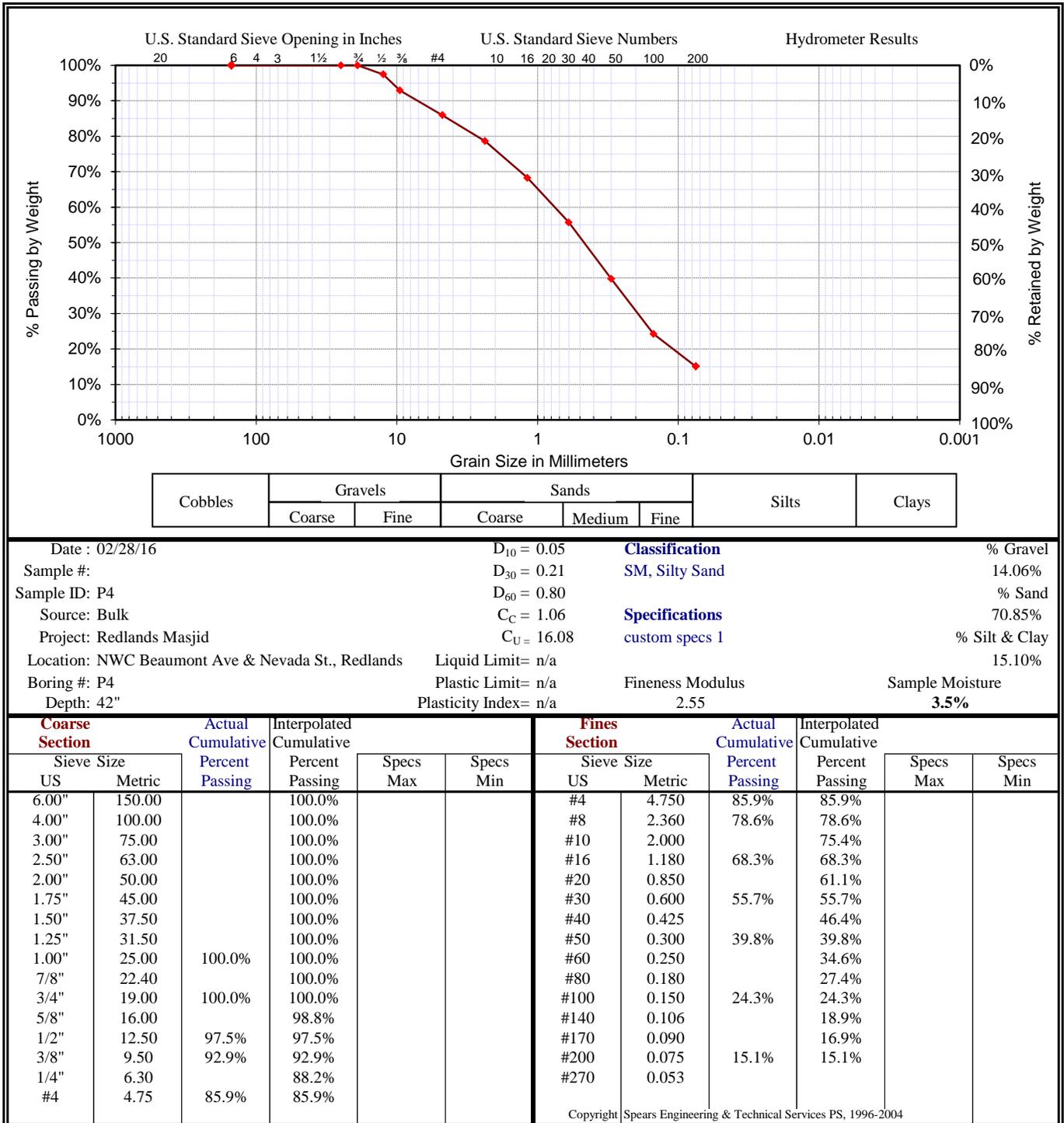
LABORATORY TEST RESULTS



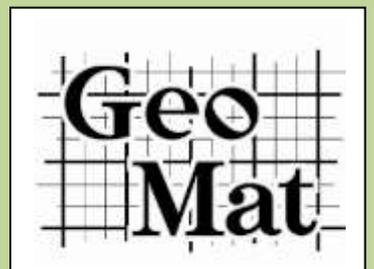
LABORATORY TEST RESULTS



LABORATORY TEST RESULTS



Appendix D



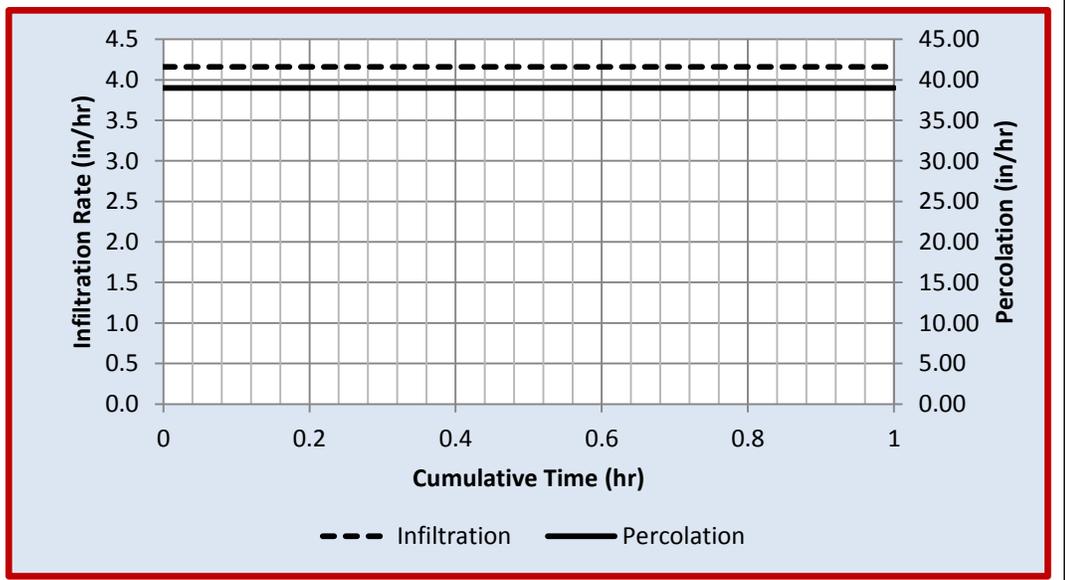
PERCOLATION TEST - P-2

Project No.	16027-01	Project Name	Redlands Masjid		
Proj. Location	Northwest Corner of Beaumont Ave and Nevada St, Redlands	Soak Method	5 gallons		
Drilling Date	2/28/2016	Soak Date	3/19/2016	Depth of Hole (in)	44
Testing Date	3/19/2016	Borehole Diameter (in)	8	Test Refill Depth (in)	20

CRITERIA	TIME	TIME INTERVAL (min)	D ₀ , INITIAL DEPTH TO WATER (in)	D _f , FINAL DEPTH TO WATER (in)	ΔH, WATER DROP (in)	AVERAGE WETTED DEPTH (in)	PERC RATE (min/in)	PERC RATE (in/hr)	CORECTED* INFILTRATION RATE (in/hr)
Sandy Soil Criteria	0:00:00	0:09:00	24	18	6				
	0:09:00	9:00							
	0:00:00	0:09:00	24	18	6				
	0:09:00	9:00							
Percolation Test Data	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
	0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16
	0:10:00	10:00							
0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16	
0:10:00	10:00								
0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16	
0:10:00	10:00								
0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16	
0:10:00	10:00								
0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16	
0:10:00	10:00								
0:00:00	0:10:00	24	30.5	6.5	16.75	1.5	39.0	4.16	
0:10:00	10:00								

*Porchet Method

Cumulative Time (hr)	Percolation (in/hr)	Infiltration (in/hr)
0	39.00	4.2
0.17	39.00	4.2
0.33	39.00	4.2
0.50	39.00	4.2
0.67	39.00	4.2
0.83	39.00	4.2
1.00	39.00	4.2



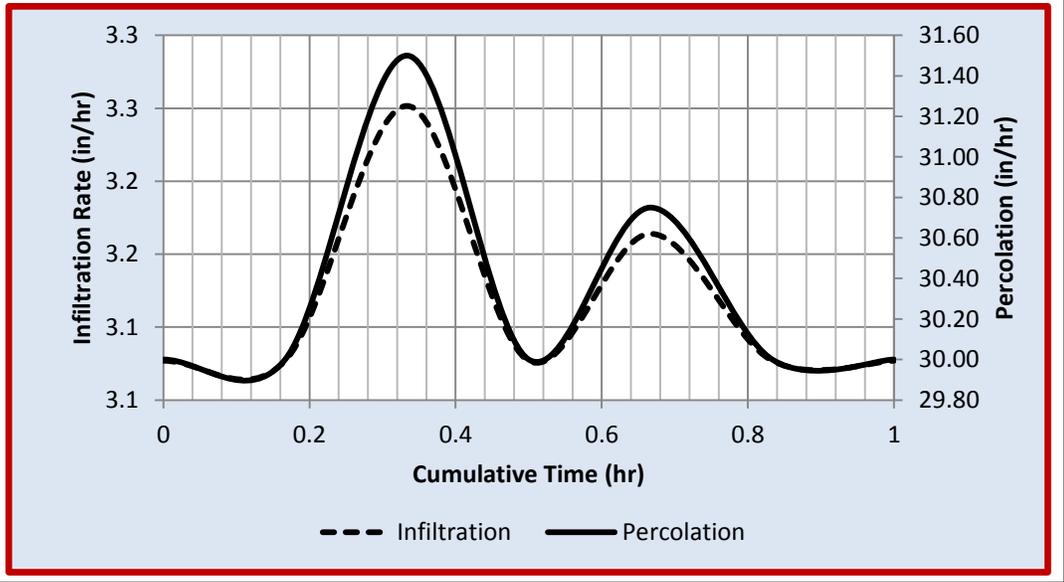
PERCOLATION TEST - P-3

Project No.	16027-01	Project Name	Redlands Masjid		
Proj. Location	Northwest Corner of Beaumont Ave and Nevada St, Redlands	Soak Method	5 gallons		
Drilling Date	2/28/2016	Soak Date	3/19/2016	Depth of Hole (in)	43
Testing Date	3/19/2016	Borehole Diameter (in)	8	Test Refill Depth (in)	20

CRITERIA	TIME	TIME INTERVAL (min)	D ₀ , INITIAL DEPTH TO WATER (in)	D _f , FINAL DEPTH TO WATER (in)	ΔH, WATER DROP (in)	AVERAGE WETTED DEPTH (in)	PERC RATE (min/in)	PERC RATE (in/hr)	CORRECTED* INFILTRATION RATE (in/hr)	
Sandy Soil Criteria	0:00:00	0:12:00	23	17	6					
	0:12:00	12:00								
	0:00:00	0:12:00	23	17	6					
	0:12:00	12:00								
Percolation Test Data	0:00:00	0:10:00	23	28	5	17.5	2.0	30.0	3.08	
	0:10:00	10:00								
	0:00:00	0:10:00	23	28.25	5.25	17.375	1.9	31.5	3.25	
	0:10:00	10:00								
	0:00:00	0:10:00	23	28	5	17.5	2.0	30.0	3.08	
	0:10:00	10:00								
	0:00:00	0:10:00	23	28.125	5.125	17.4375	2.0	30.8	3.16	
	0:10:00	10:00								
	0:00:00	0:10:00	23	28	5	17.5	2.0	30.0	3.08	
	0:10:00	10:00								
	0:00:00	0:10:00	23	28	5	17.5	2.0	30.0	3.08	
	0:10:00	10:00								

*Porchet Method

Cumulative Time (hr)	Percolation (in/hr)	Infiltration (in/hr)
0	30.00	3.1
0.17	30.00	3.1
0.33	31.50	3.3
0.50	30.00	3.1
0.67	30.75	3.2
0.83	30.00	3.1
1.00	30.00	3.1



PERCOLATION TEST - P-4

Project No.	16027-01	Project Name	Redlands Masjid		
Proj. Location	Northwest Corner of Beaumont Ave and Nevada St, Redlands	Soak Method	5 gallons		
Drilling Date	2/28/2016	Soak Date	3/19/2016	Depth of Hole (in)	42
Testing Date	3/19/2016	Borehole Diameter (in)	8	Test Refill Depth (in)	20

CRITERIA	TIME	TIME INTERVAL (min)	D ₀ , INITIAL DEPTH TO WATER (in)	D _f , FINAL DEPTH TO WATER (in)	ΔH, WATER DROP (in)	AVERAGE WETTED DEPTH (in)	PERC RATE (min/in)	PERC RATE (in/hr)	CORRECTED* INFILTRATION RATE (in/hr)	
Sandy Soil Criteria	0:00:00	0:10:00	22	16	6					
	0:10:00	10.00								
	0:00:00	0:10:00	22	16	6					
	0:10:00	10.00								
Percolation Test Data	0:00:00	0:10:00	22	28.125	6.125	16.9375	1.6	36.8	3.88	
	0:10:00	10.00								
	0:00:00	0:10:00	22	28.125	6.125	16.9375	1.6	36.8	3.88	
	0:10:00	10.00								
	0:00:00	0:10:00	22	28.125	6.125	16.9375	1.6	36.8	3.88	
	0:10:00	10.00								
	0:00:00	0:10:00	22	28.125	6.125	16.9375	1.6	36.8	3.88	
	0:10:00	10.00								
	0:00:00	0:10:00	22	28.125	6.125	16.9375	1.6	36.8	3.88	
	0:10:00	10.00								
	0:00:00	0:10:00	22	28.125	6.125	16.9375	1.6	36.8	3.88	
	0:10:00	10.00								

*Porchet Method

Cumulative Time (hr)	Percolation (in/hr)	Infiltration (in/hr)
0	36.75	3.9
0.17	36.75	3.9
0.33	36.75	3.9
0.50	36.75	3.9
0.67	36.75	3.9
0.83	36.75	3.9
1.00	36.75	3.9

