

# APPENDIX 11

## NOISE ASSESSMENT (NA)



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# **Earl Graham**

## **NOISE ANALYSIS**

### **COUNTY OF SAN BERNARDINO**

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## LIST OF ABBREVIATED TERMS

(1)	Reference
ADT	Average Daily Traffic
ANSI	American National Standards Institute
Calveno	California Vehicle Noise
CEQA	California Environmental Quality Act
CNEL	Community Noise Equivalent Level
dBA	A-weighted decibels
EPA	Environmental Protection Agency
FHWA	Federal Highway Administration
FTA	Federal Transit Administration
INCE	Institute of Noise Control Engineering
$L_{eq}$	Equivalent continuous (average) sound level
$L_{max}$	Maximum level measured over the time interval
$L_{min}$	Minimum level measured over the time interval
mph	Miles per hour
OPR	Office of Planning and Research
PPV	Peak particle velocity
Project	Earl Graham
REMEL	Reference Energy Mean Emission Level
RMS	Root-mean-square
VdB	Vibration Decibels

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## EXECUTIVE SUMMARY

Urban Crossroads, Inc. has prepared this Noise Analysis to determine the potential noise impacts and the necessary noise mitigation measures, if any, for the Earl Graham shipping container storage facility (“Project”). The Project site is located at 9233 Deep Creek Road in an unincorporated area of San Bernardino County. The Project would operate a shipping container storage facility on an approximately 42-acre parcel. This study has been prepared to demonstrate compliance with the applicable noise level standards and thresholds of significance based on guidance provided by the County of San Bernardino as informed by Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (1)

The results of this Noise Analysis are summarized below based on the significance criteria in Section 4 of this report. Table ES-1 shows the findings of significance for each potential noise and/or vibration impact under CEQA before and after any required mitigation measures.

**TABLE ES-1: SUMMARY OF CEQA SIGNIFICANCE FINDINGS**

Analysis	Report Section	Significance Findings	
		Unmitigated	Mitigated
Off-Site Traffic Noise	7	<i>Less Than Significant</i>	-
Operational Noise	8	<i>Less Than Significant</i>	-
Construction Noise	9	<i>Less Than Significant</i>	-
Construction Vibration		<i>Less Than Significant</i>	-

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# **1 INTRODUCTION**

This noise analysis has been completed to determine the noise impacts associated with the development of the Project. This noise study briefly describes the proposed Project, provides information regarding noise fundamentals, outlines the local regulatory setting, provides the study methods and procedures for performing noise analysis, evaluates potential noise impacts from the Project, and identifies mitigation measures to reduce impacts, as necessary.

## **1.1 SITE LOCATION**

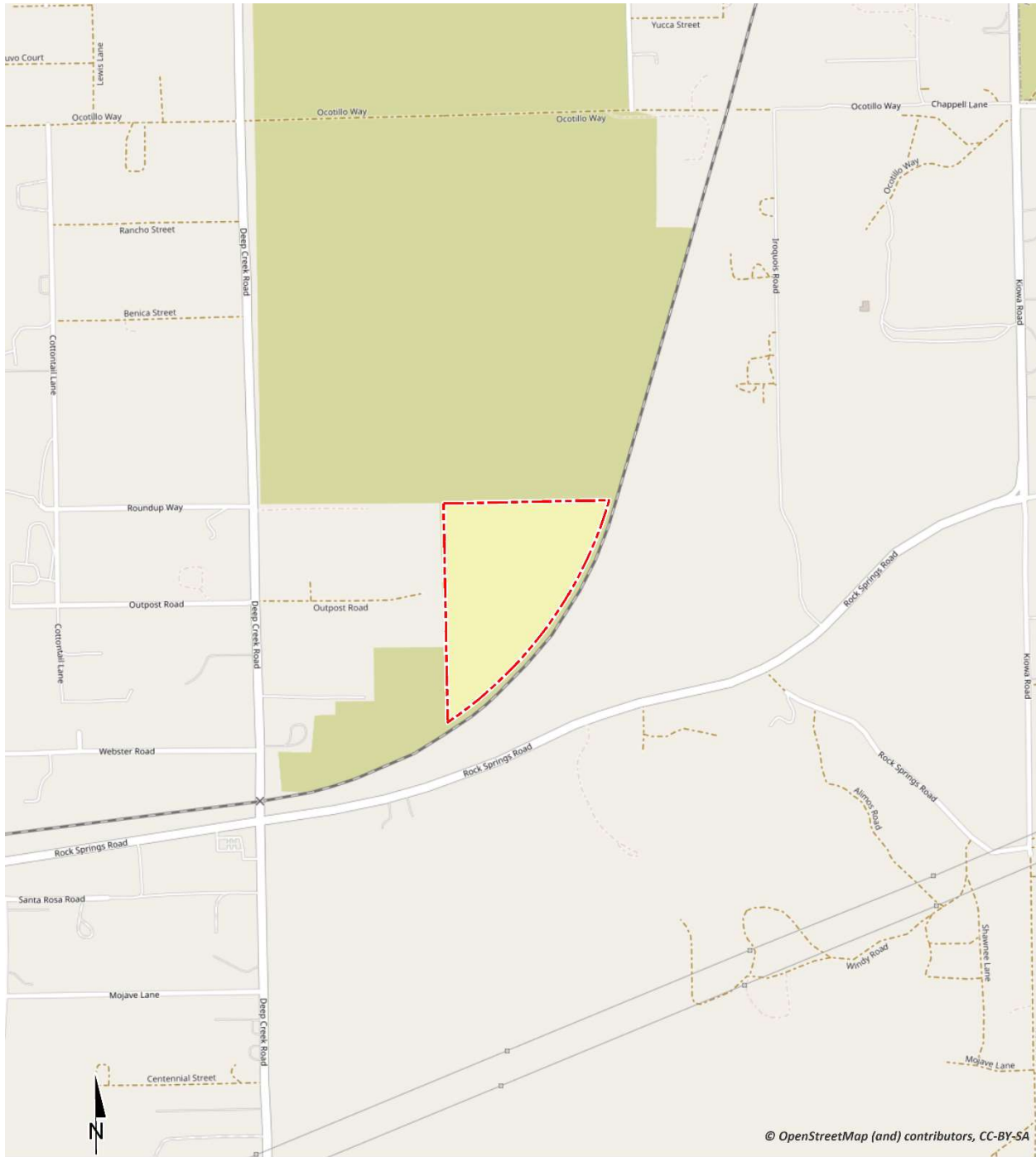
The Project site is located at 9233 Deep Creek Road in an unincorporated area of San Bernardino County. The nearest airport is the Hesperia Airport, approximately 5.83 miles to the southwest of the Project site.

The Project site is 41.71 acres and is currently undeveloped. According to the County of San Bernardino General Plan, the site's land use and zoning designation is agricultural land. The designation provides sites for commercial agricultural operations, agriculture support services, rural residential uses, and similar and compatible uses.

## **1.2 PROJECT DESCRIPTION**

The Project is to develop a shipping container storage facility. The preliminary site plan for the proposed Project is shown in Exhibit 1-B. Primary access to the site is accommodated via a main entrance on Deep Creek Road to the south. Operations will take place 24 hours a day, 7 days a week. The site would include a small trailer office, which is assumed to include an air conditioning unit. Due to the lack of structures and current site conditions, no construction is proposed. The Primary noise sources would consist of the trailer office air conditioning unit and the shipping container stacker, similar to a large loader.

### EXHIBIT 1-A: LOCATION MAP





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## 2 FUNDAMENTALS

Noise is commonly defined as “unwanted sound.” Sound becomes unwanted when it interferes with normal activities, when it causes actual physical harm, or when it has adverse effects on health. Noise is measured on a logarithmic scale of sound pressure level known as a decibel (dB). A-weighted decibels (dBA) approximate the subjective response of the human ear to broad-frequency noise sources by discriminating against very low and very high frequencies of the audible spectrum. They are adjusted to reflect only those frequencies which are audible to the human ear. Exhibit 2-A presents a summary of the typical noise levels and their subjective loudness and effects, which are described in more detail below.

**EXHIBIT 2-A: TYPICAL NOISE LEVELS**

<b>COMMON OUTDOOR ACTIVITIES</b>	<b>COMMON INDOOR ACTIVITIES</b>	<b>A - WEIGHTED SOUND LEVEL dBA</b>	<b>SUBJECTIVE LOUDNESS</b>	<b>EFFECTS OF NOISE</b>
THRESHOLD OF PAIN		140	<b>INTOLERABLE OR DEAFENING</b>	<b>HEARING LOSS</b>
NEAR JET ENGINE		130		
		120		
JET FLY-OVER AT 300m (1000 ft)	ROCK BAND	110		
LOUD AUTO HORN		100	<b>VERY NOISY</b>	<b>SPEECH INTERFERENCE</b>
GAS LAWN MOWER AT 1m (3 ft)		90		
DIESEL TRUCK AT 15m (50 ft), at 80 km/hr (50 mph)	FOOD BLENDER AT 1m (3 ft)	80	<b>LOUD</b>	
NOISY URBAN AREA, DAYTIME	VACUUM CLEANER AT 3m (10 ft)	70		
HEAVY TRAFFIC AT 90m (300 ft)	NORMAL SPEECH AT 1m (3 ft)	60	<b>MODERATE</b>	<b>SLEEP DISTURBANCE</b>
QUIET URBAN DAYTIME	LARGE BUSINESS OFFICE	50		
QUIET URBAN NIGHTTIME	THEATER, LARGE CONFERENCE ROOM (BACKGROUND)	40	<b>FAINT</b>	<b>NO EFFECT</b>
QUIET SUBURBAN NIGHTTIME	LIBRARY	30		
QUIET RURAL NIGHTTIME	BEDROOM AT NIGHT, CONCERT HALL (BACKGROUND)	20		
	BROADCAST/RECORDING STUDIO	10	<b>VERY FAINT</b>	
LOWEST THRESHOLD OF HUMAN HEARING	LOWEST THRESHOLD OF HUMAN HEARING	0		

### 2.1 RANGE OF NOISE

Since the range of intensities that the human ear can detect is so large, the scale frequently used to measure intensity is a scale based on multiples of 10, the logarithmic scale. The scale for measuring intensity is the decibel scale. Each interval of 10 decibels indicates a sound energy ten times greater than before, which is perceived by the human ear as being roughly twice as loud. (2) The most common sounds vary between 40 dBA (very quiet) to 100 dBA (very loud). Normal conversation at three feet is at roughly 60 dBA, while loud jet engine noises equate to 110 dBA at approximately 100 feet, which can cause serious discomfort. (3) Another important aspect of noise is the duration of the sound and the way it is described and distributed in time.

## 2.2 NOISE DESCRIPTORS

Environmental noise descriptors are generally based on average, rather than instantaneous, noise levels. The most used figure is the equivalent level ( $L_{eq}$ ). Equivalent sound levels are not measured directly but are calculated from sound pressure levels typically measured in A-weighted decibels (dBA). The equivalent sound level ( $L_{eq}$ ) represents a steady state sound level containing the same total energy as a time varying signal over a given sample period (typically one hour) and is commonly used to describe the “average” noise levels within the environment.

To describe the time-varying character of environmental noise, the statistical or percentile noise descriptors  $L_{50}$ ,  $L_{25}$ ,  $L_8$ , and  $L_2$ , are commonly used. The percentile noise descriptors are the noise levels equaled or exceeded during 50 percent, 25 percent, 8 percent, and 2 percent of a stated time. Sound levels associated with the  $L_2$  and  $L_8$  typically describe transient or short-term events, while levels associated with the  $L_{50}$  describe the steady state (or median) noise conditions. The  $L_n$  relies on the percentile noise levels to describe the stationary source noise level limits. While the  $L_{50}$  describes the noise levels occurring 50 percent of the time, the  $L_{eq}$  accounts for the total energy (average) observed for the entire hour.

Peak hour or average noise levels, while useful, do not completely describe a given noise environment. Noise levels lower than peak hour may be disturbing if they occur during times when quiet is most desirable, namely evening and nighttime (sleeping) hours. To account for this, the Community Noise Equivalent Level (CNEL), representing a composite 24-hour noise level is utilized. The CNEL is the weighted average of the intensity of a sound, with corrections for time of day, and averaged over 24 hours. The time-of-day corrections require the addition of 5 decibels to dBA  $L_{eq}$  sound levels in the evening from 7:00 p.m. to 10:00 p.m., and the addition of 10 decibels to dBA  $L_{eq}$  sound levels at night between 10:00 p.m. and 7:00 a.m. These additions are made to account for the noise-sensitive time periods during the evening and night hours when sound appears louder. CNEL does not represent the actual sound level heard at any time, but rather represents the total sound exposure. The County of San Bernardino relies on the 24-hour CNEL level to assess land use compatibility with transportation-related noise sources.

## 2.3 SOUND PROPAGATION

When sound propagates over a distance, it changes in level and frequency content. The way noise reduces with distance depends on the following factors.

### 2.3.1 GEOMETRIC SPREADING

Sound from a localized source (i.e., a stationary point source) propagates uniformly outward in a spherical pattern. The sound level attenuates (or decreases) at a rate of 6 dB for each doubling of distance from a point source. Highways consist of several localized noise sources on a defined path and hence can be treated as a line source, which approximates the effect of several point sources. Noise from a line source propagates outward in a cylindrical pattern, often referred to as cylindrical spreading. Sound levels attenuate at a rate of 3 dB for each doubling of distance from a line source. (2)

### 2.3.2 GROUND ABSORPTION

The propagation path of noise from a highway to a receiver is usually very close to the ground. Noise attenuation from ground absorption and reflective wave canceling adds to the attenuation associated with geometric spreading. Traditionally, the excess attenuation has also been expressed in terms of attenuation per doubling of distance. This approximation is usually sufficiently accurate for distances of less than 200 feet. For acoustically hard sites (i.e., sites with a reflective surface between the source and the receiver, such as a parking lot or body of water), no excess ground attenuation is assumed. For acoustically absorptive or soft sites (i.e., those sites with an absorptive ground surface between the source and the receiver such as soft dirt, grass, or scattered bushes and trees), an excess ground attenuation value of 1.5 dB per doubling of distance is normally assumed. When added to the cylindrical spreading, the excess ground attenuation results in an overall drop-off rate of 4.5 dB per doubling of distance from a line source. (4)

### 2.3.3 ATMOSPHERIC EFFECTS

Receivers located downwind from a source can be exposed to increased noise levels relative to calm conditions, whereas locations upwind can have lowered noise levels. Sound levels can be increased at large distances (e.g., more than 500 feet) due to atmospheric temperature inversion (i.e., increasing temperature with elevation). Other factors such as air temperature, humidity, and turbulence can also have significant effects. (2)

### 2.3.4 SHIELDING

A large object or barrier in the path between a noise source and a receiver can substantially attenuate noise levels at the receiver. The amount of attenuation provided by shielding depends on the size of the object and the frequency content of the noise source. Shielding by trees and other such vegetation typically only has an “out of sight, out of mind” effect. That is, the perception of noise impact tends to decrease when vegetation blocks the line-of-sight to nearest residents. However, for vegetation to provide a substantial, or even noticeable, noise reduction, the vegetation area must be at least 15 feet in height, 100 feet wide and dense enough to completely obstruct the line-of-sight between the source and the receiver. This size of vegetation may provide up to 5 dBA of noise reduction. The Federal Highway Administration (FHWA) does not consider the planting of vegetation to be a noise abatement measure. (4)

### 2.3.5 REFLECTION

Field studies conducted by the FHWA have shown that the reflection from barriers and buildings does not substantially increase noise levels. (4) If all the noise striking a structure was reflected back to a given receiving point, the increase would be theoretically limited to 3 dBA. Further, not all the acoustical energy is reflected back to the same point. Some of the energy would go over the structure, some is reflected to points other than the given receiving point, some is scattered by ground coverings (e.g., grass and other plants), and some is blocked by intervening structures and/or obstacles (e.g., the noise source itself). Additionally, some of the reflected energy is lost due to the longer path that the noise must travel. FHWA measurements made to quantify

reflective increases in traffic noise have not shown an increase of greater than 1-2 dBA; an increase that is not perceptible to the average human ear.

## **2.4 NOISE CONTROL**

Noise control is the process of obtaining an acceptable noise environment for an observation point or receiver by controlling the noise source, transmission path, receiver, or all three. This concept is known as the source-path-receiver concept. In general, noise control measures can be applied to these three elements.

## **2.5 NOISE BARRIER ATTENUATION**

Effective noise barriers can reduce noise levels by up to 10 to 15 dBA, cutting the loudness of traffic noise in half. A noise barrier is most effective when placed close to the noise source or receiver. Noise barriers, however, do have limitations. For a noise barrier to work, it must be high enough and long enough to block the path of the noise source. (4)

## **2.6 LAND USE COMPATIBILITY WITH NOISE**

Some land uses are more tolerant of noise than others. For example, schools, hospitals, churches, and residences are more sensitive to noise intrusion than are commercial or industrial developments and related activities. As ambient noise levels affect the perceived amenity or livability of a development, so too can the mismanagement of noise impacts impair the economic health and growth potential of a community by reducing the area's desirability as a place to live, shop and work. For this reason, land use compatibility with the noise environment is an important consideration in the planning and design process. The FHWA encourages State and Local government to regulate land development in such a way that noise-sensitive land uses are either prohibited from being located adjacent to a highway, or that the developments are planned, designed, and constructed in such a way that noise impacts are minimized. (5)

## **2.7 COMMUNITY RESPONSE TO NOISE**

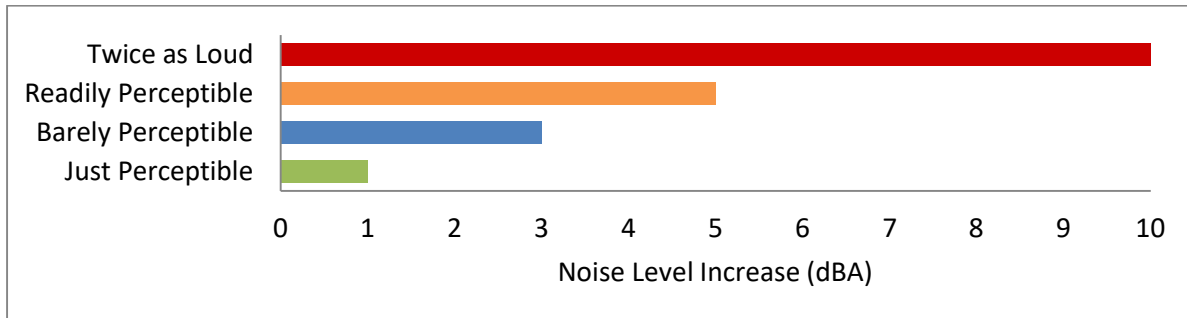
Community responses to noise may range from registering a complaint by telephone or letter, to initiating court action, depending upon everyone's susceptibility to noise and personal attitudes about noise. Several factors are related to the level of community annoyance including:

- Fear associated with noise-producing activities;
- Socio-economic status and educational level;
- Perception that those affected are being unfairly treated;
- Attitudes regarding the usefulness of the noise-producing activity;
- Belief that the noise source can be controlled.

Approximately ten percent of the population has a very low tolerance for noise and will object to any noise not of their making. Consequently, even in the quietest environment, some complaints will occur. Twenty-five percent of the population will not complain even in very severe noise environments. Thus, a variety of reactions can be expected from people exposed to any given noise environment. (6) Surveys have shown that about ten percent of the people exposed to

traffic noise of 60 dBA will report being highly annoyed with the noise, and each increase of one dBA is associated with approximately two percent more people being highly annoyed. When traffic noise exceeds 60 dBA or aircraft noise exceeds 55 dBA, people may begin to complain. (6) Despite this variability in behavior on an individual level, the population can be expected to exhibit the following responses to changes in noise levels as shown on Exhibit 2-B. A change of 3 dBA is considered *barely perceptible*, and changes of 5 dBA are considered *readily perceptible*. (4)

**EXHIBIT 2-B: NOISE LEVEL INCREASE PERCEPTION**



## 2.8 VIBRATION

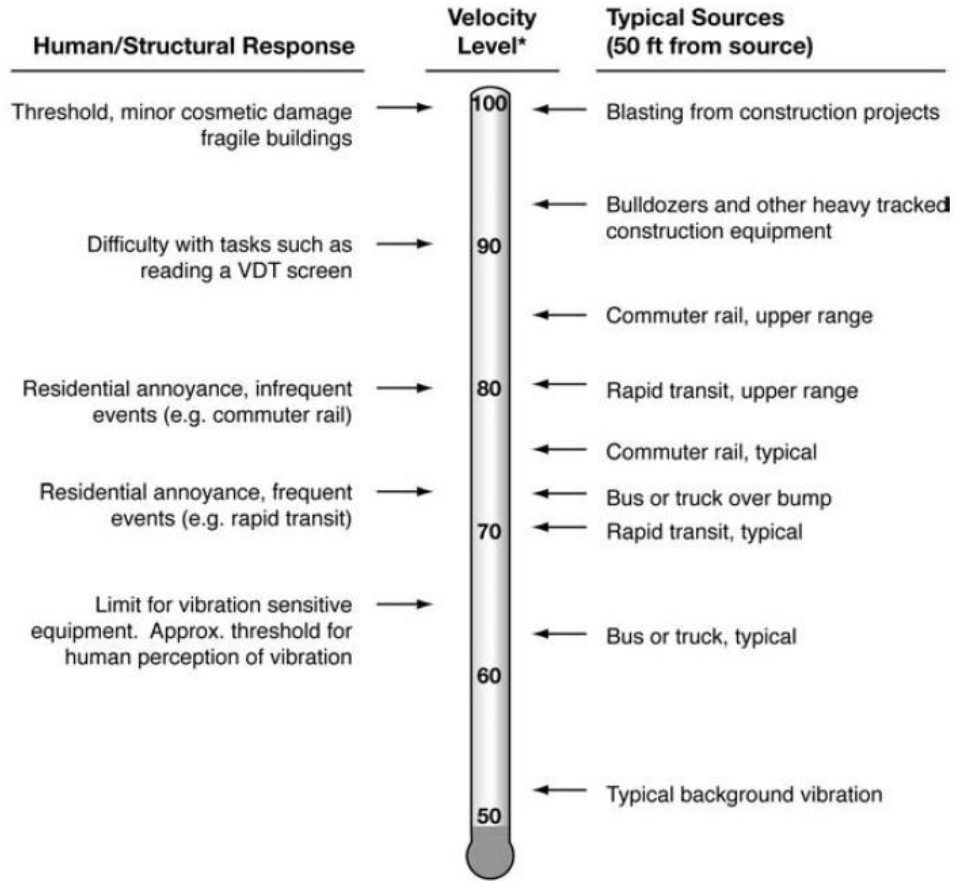
As defined in the Federal Transit Administration (FTA) *Transit Noise and Vibration Impact Assessment Manual* (7) and the California Department of Transportation (Caltrans) *Transportation and Construction Vibration Guidance Manual*, vibration is the periodic oscillation of a medium or object. The rumbling sound caused by the vibration of room surfaces is called structure-borne noise. Sources of ground-borne vibrations include natural phenomena (e.g., earthquakes, volcanic eruptions, sea waves, landslides) or human-generated sources (e.g., explosions, machinery, traffic, trains, construction equipment). Vibration sources may be continuous, such as factory machinery, or transient, such as explosions or train pass-bys. As is the case with airborne sound, ground-borne vibrations may be described by amplitude and frequency. Groundborne vibration is primarily a concern inside structures, and is almost never a problem outside of structures (7). Additionally, ground-borne vibration generated by man-made activities typically attenuates rapidly with distance from the source of the vibration. Sensitive receivers for vibration include older stone, adobe, and masonry structures, places where people reside (especially residents, the elderly, and sick), and vibration-sensitive equipment and/or activities.

There are several different methods that are used to quantify vibrations. The peak particle velocity (PPV) in inches per second (in/sec) is the most common and is defined as the maximum instantaneous peak of the vibration signal. The PPV was developed primarily to describe vibration impacts to buildings and is not always the most suitable for evaluating human response to vibration because it takes some time for the human body to respond to vibration signals. Instead, the human body responds to average vibration amplitude often described as the root

mean square (RMS) amplitude in in/sec. The RMS amplitude is defined as the average of the squared amplitude of the signal and may be more appropriate for describing the effect of vibration on the human body. However, the RMS amplitude and PPV are related mathematically, and the RMS amplitude can be calculated from the PPV. The RMS amplitude is approximately 70% of the PPV (8).

While not universally accepted, vibration decibel notation (VdB) is used by the FTA in their guidance manual to describe vibration levels and provide a background of common vibration levels (7). As stated in the FTA guidance manual, the background vibration-velocity level in residential areas is generally 50 VdB. Ground-borne vibration is normally perceptible to humans at approximately 65 VdB. For most people, a vibration-velocity level of 75 VdB is the approximate dividing line between barely perceptible and distinctly perceptible levels. Typical outdoor sources of perceptible ground-borne vibration are construction equipment, steel-wheeled trains, and traffic on rough roads. If a roadway is smooth, the ground-borne vibration is rarely perceptible. The range of interest is from approximately 50 VdB, which is the typical background vibration-velocity level, to 100 VdB, which is the general threshold where minor damage can occur in fragile buildings. Exhibit 2-C illustrates common vibration sources and the human and structural response to ground-borne vibration.

**EXHIBIT 2-C: TYPICAL LEVELS OF GROUND-BORNE VIBRATION**



\* RMS Vibration Velocity Level in VdB relative to 10<sup>-6</sup> inches/second

Source: Federal Transit Administration (FTA) Transit Noise and Vibration Impact Assessment Manual.

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### 3 REGULATORY SETTING

To limit population exposure to physically and/or psychologically damaging as well as intrusive noise levels, the federal government, the State of California, various county governments, and most municipalities in the state have established standards and ordinances to control noise. In most areas, automobile and truck traffic is the major source of environmental noise. Traffic activity generally produces an average sound level that remains constant with time. Air and rail traffic, and commercial and industrial activities are also major sources of noise in some areas. Federal, state, and local agencies regulate different aspects of environmental noise. Federal and state agencies generally set noise standards for mobile sources such as aircraft and motor vehicles, while regulation of stationary sources is left to local agencies.

#### 3.1 STATE OF CALIFORNIA NOISE REQUIREMENTS

The State of California regulates freeway noise, sets standards for sound transmission, provides occupational noise control criteria, identifies noise standards, and provides guidance for local land use compatibility. State law requires that each county and city adopt a General Plan that includes a Noise Element which is to be prepared per guidelines adopted by the Governor's Office of Planning and Research (OPR). (9) The purpose of the Noise Element is to *limit the exposure of the community to excessive noise levels*. In addition, the California Environmental Quality Act (CEQA) requires that all known environmental effects of a project be analyzed, including environmental noise impacts.

#### 3.2 COUNTY OF SAN BERNARDINO GENERAL PLAN NOISE ELEMENT

The County of San Bernardino has adopted a Noise Element of the General Plan to limit the exposure of the community to excessive noise levels. (10) The most common sources of environmental noise in San Bernardino County are associated with roads, airports, railroad operations, and industrial activities. The facilities are used to transport residents, consumer products, and provide basic infrastructure for the community. (10) To address these noise sources found in the County of San Bernardino, the following goals have been identified in the General Plan Noise Element:

- N 1 *The County will abate and avoid excessive noise exposures through noise mitigation measures incorporated into the design of new noise-generating and new noise-sensitive land uses, while protecting areas within the County where the present noise environment is within acceptable limits.*
- N 1.3 *When industrial, commercial, or other land uses, including locally regulated noise sources, are proposed for areas containing noise-sensitive land uses, noise levels generated by the proposed use will not exceed the performance standards of Table N-2 within outdoor activity areas. If outdoor activity areas have not yet been determined, noise levels shall not exceed the performance standards listed in Chapter 83.01 of the Development Code at the boundary of areas planned or zoned for residential or other noise-sensitive land uses.*

- N 1.5 Limit truck traffic in residential and commercial areas to designated truck routes; limit construction, delivery, and through-truck traffic to designated routes; and distribute maps of approved truck routes to County traffic officers.*
- N 1.6 Enforce the hourly noise-level performance standards for stationary and other locally regulated sources, such as industrial, recreational, and construction activities as well as mechanical and electrical equipment.*
- N 2 The County will strive to preserve and maintain the quiet environment of mountain, desert and other rural areas.*
- N 2.1 The County will require appropriate and feasible on-site noise attenuating measures that may include noise walls, enclosure of noise generating equipment, site planning to locate noise sources away from sensitive receptors, and other comparable features.*

### **3.3 COUNTY OF SAN BERNARDINO DEVELOPMENT CODE**

While the County of San Bernardino General Plan Noise Element provides guidelines and criteria to assess transportation noise on sensitive land uses, the County Code, Title 8 Development Code contains the noise level limits for mobile, stationary, and construction-related noise sources. (11)

#### **3.3.1 TRANSPORTATION NOISE STANDARDS**

Section 83.01.080(d), Table 83-3, contains the County of San Bernardino's mobile noise source-related standards, shown on Exhibit 3-A. Based on the County's mobile noise source standards, there are no exterior noise level standards for the Project commercial land use. Exterior transportation (mobile) noise level standards for residential land uses in the Project study area are shown to be 60 dBA CNEL, while non-noise-sensitive land uses, such as office uses, require exterior noise levels of 65 dBA CNEL per the County's Table 83-3 mobile noise source standards.

#### **3.3.2 OPERATIONAL NOISE STANDARDS**

The noise impacts originating from a designated fixed location stationary noise-sources are typically evaluated against standards established under a jurisdiction's Code. The County of San Bernardino County, Development Code, Title 8, Section 83.01.080(c) establishes the noise level standards for stationary noise sources. Since the Project's land use will potentially impact adjacent noise-sensitive uses in the Project study area, this noise study relies on the more conservative residential noise level standards to describe potential operational noise impacts.

**EXHIBIT 3-A: COUNTY OF SAN BERNARDINO MOBILE NOISE LEVEL STANDARDS**

<b>Noise Standards for Adjacent Mobile Noise Sources</b>			
<b>Land Use</b>		<b>Ldn (or CNEL) dB(A)</b>	
<b>Categories</b>	<b>Uses</b>	<b>Interior (1)</b>	<b>Exterior (2)</b>
Residential	Single and multi-family, duplex, mobile homes	45	60(3)
Commercial	Hotel, motel, transient housing	45	60(3)
	Commercial retail, bank, restaurant	50	N/A
	Office building, research and development, professional offices	45	65
	Amphitheater, concert hall, auditorium, movie theater	45	N/A
Institutional/Public	Hospital, nursing home, school classroom, religious institution, library	45	65
Open Space	Park	N/A	65

Notes:

(1) The indoor environment shall exclude bathrooms, kitchens, toilets, closets and corridors.

(2) The outdoor environment shall be limited to:

- Hospital/office building patios
- Hotel and motel recreation areas
- Mobile home parks
- Multi-family private patios or balconies
- Park picnic areas
- Private yard of single-family dwellings
- School playgrounds

(3) An exterior noise level of up to 65 dB(A) (or CNEL) shall be allowed provided exterior noise levels have been substantially mitigated through a reasonable application of the best available noise reduction technology, and interior noise exposure does not exceed 45 dB(A) (or CNEL) with windows and doors closed. Requiring that windows and doors remain closed to achieve an acceptable interior noise level shall necessitate the use of air conditioning or mechanical ventilation.

CNEL = (Community Noise Equivalent Level). The average equivalent A-weighted sound level during a 24-hour day, obtained after addition of approximately five decibels to sound levels in the evening from 7:00 p.m. to 10:00 p.m. and ten decibels to sound levels in the night from 10:00 p.m. to 7:00 a.m.

Source: County of San Bernardino County Code, Title 8 Development Code, Table 83-3.

For residential properties, the exterior noise level shall not exceed 55 dBA  $L_{eq}$  during the daytime hours (7:00 a.m. to 10:00 p.m.) and 45 dBA  $L_{eq}$  during the nighttime hours (10:00 p.m. to 7:00 a.m.) for both the whole hour, and for not more than 30 minutes in any hour. (11) The exterior noise level standards shall apply for a cumulative period of 30 minutes in any hour, as well as the standard plus 5 dBA cannot be exceeded for a cumulative period of more than 15 minutes in any hour, or the standard plus 10 dBA for a cumulative period of more than 5 minutes in any hour, or the standard plus 15 dBA for a cumulative period of more than 1 minute in any hour, or the standard plus 20 dBA for any period of time. Further, Section 83.01.080(e) indicates that if the existing ambient noise level already exceeds any of the exterior noise level limit categories, then the standard shall be adjusted to reflect the ambient conditions. The County of San Bernardino operational noise level standards are shown in Table 3-1 and included in Appendix 3.1.

**TABLE 3-1: OPERATIONAL NOISE LEVEL STANDARDS**

Affected Land Uses (Receiving Noise)	Period	(dBA Leq)				
		30 min	15 min	5 min	1 min	L <sub>max</sub>
Residential	7:00 a.m. - 10:00 p.m.	55	60	65	70	75
	10:00 p.m. - 7:00 a.m.	45	50	55	60	65
Professional Services	Anytime	55	60	65	70	75
Other Commercial		60	65	70	75	80
Industrial		70	75	80	85	90

L<sub>eq</sub> = (Equivalent Energy Level). The sound level corresponding to a steady-state sound level containing the same total energy as a time-varying signal over a given sample period, e.g., 1-hour, 30-minutes, 15-minutes, etc.

L<sub>max</sub> = maximum noise level

dB(A) = (A-weighted Sound Pressure Level). The sound pressure level, in decibels, as measured on a sound level meter using the A-weighting filter network. The A-weighting filter de-emphasizes the very low and very high-frequency components of the sound, placing greater emphasis on those frequencies within the sensitivity range of the human ear.

The percentile noise descriptors are provided to ensure that the duration of the noise source is fully considered. However, due to the relatively constant intensity of the Project operational activities, the L<sub>50</sub> or average L<sub>eq</sub> noise level metrics best describe the noise sources associated with the Project. In addition, the L<sub>eq</sub> noise level metric accounts for noise fluctuations over time by averaging the louder and quieter events and giving more weight to the louder events. In addition, due to the mathematical relationship between the median (L<sub>50</sub>) and the mean (L<sub>eq</sub>), the L<sub>eq</sub> will always be larger than or equal to the L<sub>50</sub>. The more variable the noise becomes, the larger the L<sub>eq</sub> becomes in comparison to the L<sub>50</sub>. Therefore, this noise study conservatively relies on the average L<sub>eq</sub> sound level limits to describe the Project operational noise levels.

## 4 SIGNIFICANCE CRITERIA

The following significance criteria are based on currently adopted guidance provided by Appendix G of the California Environmental Quality Act (CEQA) Guidelines. (9) For the purposes of this report, impacts would be potentially significant if the Project results in or causes:

- A. Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?
- B. Generation of excessive ground-borne vibration or ground-borne noise levels?
- C. For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

While the County of San Bernardino General Plan Guidelines provide direction on noise compatibility and establish noise standards by land use type that are sufficient to assess the significance of noise impacts, they do not define the levels at which increases are considered substantial for use under Guideline A. CEQA Appendix G Guideline C applies to nearby public and private airports, if any, and the Project's land use compatibility.

### 4.1 NOISE LEVEL INCREASES (THRESHOLD A)

Noise level increases resulting from the Project are evaluated based on the Appendix G CEQA Guidelines. Under CEQA, consideration must be given to the magnitude of the increase, the existing baseline ambient noise levels, and the location of receivers to determine if a noise increase represents a significant adverse environmental impact. This approach recognizes *that there is no single noise increase that renders the noise impact significant*. (14) This is primarily because of the wide variation in individual thresholds of annoyance and differing individual experiences with noise. In general, the more a new noise level exceeds the previously existing ambient noise level, the less acceptable the new noise level will typically be judged. Thus, an important way of determining a person's subjective reaction to a new noise is the comparison of it to the existing environment to which one has adapted—the so-called *ambient* environment. The *ambient noise level* is the composite of noise from all sources, excluding the alleged offensive noise. In this context, it represents the normal or existing level of environmental noise at a given location for a specified time of day or night.

#### 4.1.1 TRANSPORTATION NOISE (SUBSTANTIAL PERMANENT NOISE LEVEL INCREASE)

The Federal Interagency Committee on Noise (FICON) (15) developed guidance to be used for the assessment of project-generated increases in noise levels that consider the ambient noise level. The FICON recommendations are based on studies that relate aircraft noise levels to the percentage of persons highly annoyed by aircraft noise. Although the FICON recommendations were specifically developed to assess aircraft noise impacts, these recommendations are often used in environmental noise impact assessments involving the use of cumulative noise exposure metrics, such as the average-daily noise level (CNEL) and equivalent continuous noise level ( $L_{eq}$ ).

As previously stated, the approach used in this noise study recognizes *that there is no single noise increase that renders a noise impact significant*, based on a 2008 California Court of Appeal ruling on Gray v. County of Madera. (14) For example, if the ambient noise environment is quiet (<60 dBA) and the new noise source greatly increases the noise levels, an impact may occur if the noise criteria may be exceeded. Therefore, for this analysis, a *readily perceptible* 5 dBA or greater project-related noise level increase is considered a significant impact when the without project noise levels are below 60 dBA. Per the FICON, in areas where the without project noise levels range from 60 to 65 dBA, a 3 dBA *barely perceptible* noise level increase appears to be appropriate for most people. When the without project noise levels already exceed 65 dBA, any increase in community noise louder than 1.5 dBA or greater is considered a significant impact if the noise criteria for a given land use is exceeded, since it likely contributes to an existing noise exposure exceedance.

The FICON guidance provides an established source of criteria to assess the impacts of substantial permanent increase in baseline ambient noise levels. Based on the FICON criteria, the amount to which a given noise level increase is considered acceptable is reduced when the without Project (baseline) noise levels are already shown to exceed certain land-use specific exterior noise level criteria. The specific levels are based on typical responses to noise level increases of 5 dBA or *readily perceptible*, 3 dBA or *barely perceptible*, and 1.5 dBA depending on the underlying without Project noise levels for noise-sensitive uses. These levels of increases and their perceived acceptance at noise sensitive receiver locations are consistent with guidance provided by both the Federal Highway Administration (5 p. 9) and Caltrans (16 p. 2\_48).

The County of San Bernardino General Plan Noise Element, *Noise Compatibility by Land Use Type* was used to establish the satisfactory noise levels of significance for non-noise-sensitive land uses in the Project study area. As previously shown on Exhibit 3-A, the *completely compatible* exterior noise level for non-noise-sensitive land uses is 70 dBA CNEL. To determine if Project-related traffic noise level increases are significant at off-site non-noise-sensitive land uses, a *barely perceptible* 3 dBA criteria is used. When the without Project noise levels are greater than the *completely compatible* 70 dBA CNEL land use compatibility criteria, a *barely perceptible* 3 dBA or greater noise level increase is considered a significant impact since the noise level criteria is already exceeded. The noise level increases used to determine significant impacts for non-noise-sensitive land uses is generally consistent with the FICON noise level increase thresholds for noise-sensitive land uses but instead rely on the County of San Bernardino General Plan Noise Element, *Noise Compatibility by Land Use Type completely compatible* 70 dBA CNEL exterior noise level criteria.

#### **4.1.2 NON-TRANSPORTATION NOISE (SUBSTANTIAL PERMANENT NOISE LEVEL INCREASE)**

The FICON criteria are also used to determine if Project-related stationary source (operational) noise level increases are significant at off-site receiver locations. For non-transportation noise source activities, a substantial permanent noise level increase consists of increases of 5 dBA or *readily perceptible*, 3 dBA or *barely perceptible*, and 1.5 dBA depending on the underlying ambient noise levels.

## 4.2 VIBRATION (GUIDELINE B)

As described in Section 3.5, vibration-generating activities are appropriately evaluated using the Caltrans vibration damage thresholds to assess potential temporary construction-related impacts at adjacent building locations. The nearest noise sensitive buildings adjacent to the Project site can best be described as “older residential structures” with a maximum acceptable continuous vibration threshold of 0.2 PPV (in/sec).

## 4.3 CEQA GUIDELINES NOT FURTHER ANALYZED (GUIDELINE C)

CEQA Noise Threshold C applies when there are nearby public and private airports and/or air strips and focuses on land use compatibility of the Project to nearby airports and airstrips. The Project site is not located within two miles of an airport or airstrip. The closest airport is the Hesperia Airport located approximately 5.83 miles southwest of the Project site. As such, the Project site would not be exposed to excessive noise levels from airport operations, and therefore, impacts are considered *less than significant*, and no further noise analysis is conducted in relation to Appendix G to the CEQA Guidelines, Noise Threshold C.

## 4.4 SIGNIFICANCE CRITERIA SUMMARY

Noise impacts shall be considered significant if any of the following occur as a direct result of the proposed Project. Table 4-1 shows the significance criteria summary matrix.

**TABLE 4-1: SIGNIFICANCE CRITERIA SUMMARY**

Analysis	Land Use	Condition(s)	Significance Criteria	
			Daytime	Nighttime
Operational	Residential	Exterior Noise Level Limit <sup>1</sup>	55 dBA L <sub>eq</sub>	45 dBA L <sub>eq</sub>
	Noise-Sensitive <sup>2</sup>	if ambient is < 60 dBA L <sub>eq</sub>	≥ 5 dBA L <sub>eq</sub> Project increase	
		if ambient is 60 - 65 dBA L <sub>eq</sub>	≥ 3 dBA L <sub>eq</sub> Project increase	
		if ambient is > 65 dBA L <sub>eq</sub>	≥ 1.5 dBA L <sub>eq</sub> Project increase	

<sup>1</sup> County of San Bernardino Development Code, Title 8, Section 83.01.080 (Appendix 3.1)

<sup>2</sup> FICON, 1992.

"Daytime" = 7:00 a.m. to 7:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

## 5 EXISTING NOISE LEVEL MEASUREMENTS

To assess the existing noise level environment, 24-hour noise level measurements were taken at five locations in the Project study area. The receiver locations were selected to describe and document the existing noise environment within the Project study area. Exhibit 5-A provides the boundaries of the Project study area and the noise level measurement locations. To fully describe the existing noise conditions, noise level measurements were collected by Urban Crossroads, Inc. on Wednesday, July 24, 2024. Appendix 5.1 includes study area photos.

### 5.1 MEASUREMENT PROCEDURE AND CRITERIA

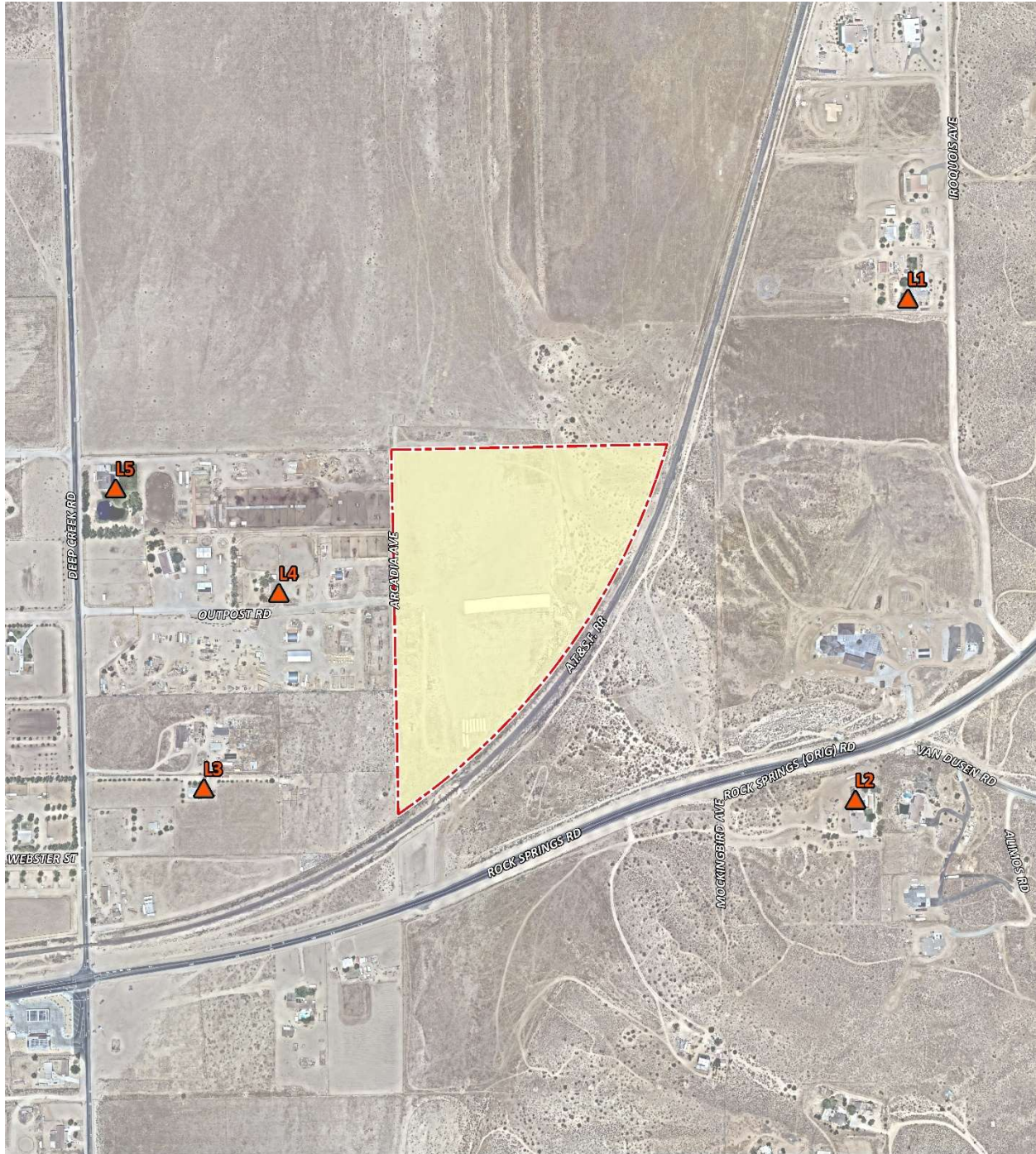
To describe the existing noise environment, the hourly noise levels were measured during typical weekday conditions over a 24-hour period. By collecting individual hourly noise level measurements, it is possible to describe the daytime and nighttime hourly noise levels and calculate the 24-hour CNEL. The long-term noise readings were recorded using Piccolo Type 2 integrating sound level meter and dataloggers. The Piccolo sound level meters were calibrated using a Larson-Davis calibrator, Model CAL 150. All noise meters were programmed in “slow” mode to record noise levels in “A” weighted form. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (16)

### 5.2 NOISE MEASUREMENT LOCATIONS

The long-term noise level measurements were positioned as close to the nearest sensitive receiver locations as possible to assess the existing ambient hourly noise levels surrounding the Project site. Both Caltrans and the FTA recognize that it is not reasonable to collect noise level measurements that can fully represent every part of a private yard, patio, deck, or balcony normally used for human activity when estimating impacts for new development projects. This is demonstrated in the Caltrans general site location guidelines which indicate that, *sites must be free of noise contamination by sources other than sources of interest. Avoid sites located near sources such as barking dogs, lawnmowers, pool pumps, and air conditioners unless it is the express intent of the analyst to measure these sources.* (2) Further, FTA guidance states, *that it is not necessary nor recommended that existing noise exposure be determined by measuring at every noise-sensitive location in the project area. Rather, the recommended approach is to characterize the noise environment for clusters of sites based on measurements or estimates at representative locations in the community.* (7)

Based on recommendations of Caltrans and the FTA, it is not necessary to collect measurements at each individual building or residence, because each receiver measurement represents a group of buildings that share acoustical equivalence. (7) In other words, the area represented by the receiver shares similar shielding, terrain, and geometric relationship to the reference noise source. Receivers represent a location of noise sensitive areas and are used to estimate the future noise level impacts.

EXHIBIT 5-A: NOISE MEASUREMENT LOCATIONS



**LEGEND:**  
N [North Arrow] [Red Dashed Box] Site Boundary [Orange Triangle] Measurement Locations

Collecting reference ambient noise level measurements at the nearby sensitive receiver locations allows for a comparison of the before and after Project noise levels and is necessary to assess potential noise impacts due to the Project's contribution to the ambient noise levels.

### 5.3 NOISE MEASUREMENT RESULTS

The noise measurements presented below focus on the average or equivalent sound levels ( $L_{eq}$ ). The equivalent sound level ( $L_{eq}$ ) represents a steady-state sound level containing the same total energy as a time-varying signal over a given sample period. Table 5-1 identifies the hourly daytime (7:00 a.m. to 10:00 p.m.) and nighttime (10:00 p.m. to 7:00 a.m.) noise levels at each noise level measurement location.

**TABLE 5-1: 24-HOUR AMBIENT NOISE LEVEL MEASUREMENTS**

Location <sup>1</sup>	Description	Energy Average Noise Level (dBA $L_{eq}$ ) <sup>2</sup>	
		Daytime	Nighttime
L1	Located northeast of the site near the residence at 9426 Iroquois Ave.	51.7	43.3
L2	Located southeast of the site near the residence at 20535 Rock Springs Rd.	52.9	50.3
L3	Located west of the site near the residence at 9141 Deep Creek Rd.	59.0	53.8
L4	Located west of the site near the residence at 20276 Outpost Rd.	62.3	58.8
L5	Located west of the site near the residence at 9293 Deep Creek Rd.	69.5	65.0

<sup>1</sup> See Exhibit 5-A for the noise level measurement locations.

<sup>2</sup> Energy (logarithmic) average levels. The long-term 24-hour measurement worksheets are included in Appendix 5.2. "Daytime" = 7:00 a.m. to 7:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

Table 5-1 provides the (energy average) noise levels used to describe the daytime and nighttime ambient conditions. These daytime and nighttime energy average noise levels represent the average of all hourly noise levels observed during these time periods expressed as a single number. Appendix 5.2 provides summary worksheets of the noise levels for each hour as well as the minimum, maximum,  $L_1$ ,  $L_2$ ,  $L_5$ ,  $L_8$ ,  $L_{25}$ ,  $L_{50}$ ,  $L_{90}$ ,  $L_{95}$ , and  $L_{99}$  percentile noise levels observed during the daytime and nighttime periods.]

The background ambient noise levels in the Project study area are dominated by the transportation-related noise associated with surface streets in addition to background industrial land use activities. This includes the auto and truck activities on study area roadway segments near the noise level measurement locations.

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## 6 SENSITIVE RECEIVER LOCATIONS

To assess the potential for long-term operational and short-term construction noise impacts, the following sensitive receiver locations, as shown in Exhibit 6-A, were identified as representative locations for analysis. Sensitive receivers are generally defined as locations where people reside or where the presence of unwanted sound could otherwise adversely affect the use of the land. Noise-sensitive land uses are generally considered to include schools, hospitals, single-family dwellings, mobile home parks, churches, libraries, and recreation areas. Moderately noise-sensitive land uses typically include multi-family dwellings, hotels, motels, dormitories, outpatient clinics, cemeteries, golf courses, country clubs, athletic/tennis clubs, and equestrian clubs. Land uses that are considered relatively insensitive to noise include business, commercial, and professional developments. Land uses that are typically not affected by noise include: industrial, manufacturing, utilities, agriculture, undeveloped land, parking lots, warehousing, liquid and solid waste facilities, salvage yards, and transit terminals.

To describe the potential off-site Project noise levels, four receiver locations in the vicinity of the Project site were identified. All distances are measured from the Project site boundary to the outdoor living areas (e.g., private backyards), Project boundary line, or at the building façade, whichever is closer to the Project site. The selection of receiver locations is based on FHWA guidelines and is consistent with additional guidance provided by Caltrans and the FTA, as previously described in Section 5.2. Other sensitive land uses in the Project study area that are located at greater distances than those identified in this noise study will experience lower noise levels than those presented in this report due to the additional attenuation from distance and the shielding of intervening structures. Distance is measured in a straight line from the project boundary to each receiver location.

- R1: Location R1 represents an existing noise sensitive residence located at 9426 Iroquois Avenue, approximately 1,159 feet to the northeast of the Project site. A 24-hour noise measurement was taken near this location, L1, to describe the existing ambient noise environment.
- R2: Location R2 represents an existing noise sensitive residence located at 20535 Rock Springs Road, approximately 1,329 feet to the southeast of the Project site. A 24-hour noise measurement was taken near this location, L2, to describe the existing ambient noise environment.
- R3: Location R3 represents an existing noise sensitive residence located at 9141 Deep Creek Road, approximately 801 feet to the southwest of the Project site. A 24-hour noise measurement was taken near this location, L3, to describe the existing ambient noise environment.
- R4: Location R4 represents an existing noise sensitive residence located at 20276 Outpost Road, approximately 475 feet to the west of the Project site. A 24-hour noise measurement was taken near this location, L4, to describe the existing ambient noise environment.

R5: Location R5 represents an existing noise sensitive residence located at 9293 Deep Creek Road, approximately 1,138 feet to the west of the Project site. A 24-hour noise measurement was taken near this location, L5, to describe the existing ambient noise environment.

**EXHIBIT 6-A: SENSITIVE RECEIVER LOCATIONS**



## 7 OFF-SITE TRAFFIC NOISE IMPACTS

The Project would result in a small increase in regional and local traffic volumes. The Project is anticipated to generate a maximum of 246 two-way trip-ends per day (17), which would represent an incremental increase to the existing roadway volumes of 1,147 ADT and 10,278 ADT for Deep Creek Road and Rock Springs Road, respectively (18), and is not expected to generate a perceptible noise level increase (i.e., less than 3 dBA CNEL) at nearby sensitive land uses adjacent to study area roadways. Due to the low traffic volumes generated by the Project, the off-site traffic noise levels generated by the Project are considered *less than significant*.

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## 8 OPERATIONAL NOISE IMPACTS

This section analyzes the potential stationary-source operational noise impacts at the nearest receiver locations, identified in Section 6, resulting from the operation of the Project. Exhibit 8-A identifies the representative noise source locations used to assess the hourly average  $L_{eq}$  operational noise levels consistent with the County of San Bernardino noise standards. Appendix 8.1 includes the detailed calculations for the Project operational noise levels presented in this section.

### 8.1 OPERATIONAL NOISE SOURCES

This operational noise analysis is intended to describe noise level impacts associated with the expected typical daytime and nighttime activities at the Project site. To present the potential worst-case noise conditions, this analysis assumes the Project would be operational 24 hours per day, seven days per week. The on-site Project-related noise sources are expected to include: air conditioning unit.

### 8.2 REFERENCE NOISE LEVELS

To estimate the Project operational noise impacts, reference noise levels were taken from manufacturer's specifications or measurements were collected from similar types of activities to represent the noise levels expected with the development of the proposed Project. This section provides a detailed description of the reference noise level measurements shown in Table 8-1 used to estimate the Project operational noise impacts. It is important to note that the following projected noise levels assume the worst-case noise environment with air conditioning unit all operating at the same time. These sources of noise activity will likely vary throughout the day.

#### 8.2.1 MEASUREMENT PROCEDURES

The reference noise level measurements presented in this section were collected using a Larson Davis LxT Type 1 precision sound level meter (serial number 01146). The LxT sound level meter was calibrated using a Larson-Davis calibrator, Model CAL 200, was programmed in "slow" mode to record noise levels in "A" weighted form and was located at approximately five feet above the ground elevation for each measurement. The sound level meters and microphones were equipped with a windscreen during all measurements. All noise level measurement equipment satisfies the American National Standards Institute (ANSI) standard specifications for sound level meters ANSI S1.4-2014/IEC 61672-1:2013. (16)

**EXHIBIT 8-A: OPERATIONAL NOISE SOURCE LOCATIONS**



**LEGEND:**

-  Roof-Top Air Conditioning Unit
-  Shipping Container Storage

**TABLE 8-1: REFERENCE NOISE LEVEL MEASUREMENTS**

Noise Source <sup>1</sup>	Noise Source Height (Feet)	Min./Hour <sup>2</sup>		Reference Noise Level (dBA L <sub>eq</sub> ) @ 50 Feet	Sound Power Level (dBA) <sup>3</sup>
		Day	Night		
Air Conditioning	3'	45'	30'	52.1	83.7
Container Storage Activity	5'	60'	0'	71.8	103.4

<sup>1</sup> As measured by Urban Crossroads, Inc.

<sup>2</sup> Anticipated duration (minutes within the hour) of noise activity during typical hourly conditions expected at the Project site. "Daytime" = 7:00 a.m. to 7:00 p.m.; "Nighttime" = 10:00 p.m. to 7:00 a.m.

<sup>3</sup> Sound power level represents the total amount of acoustical energy (noise level) produced by a sound source independent of distance or surroundings. Sound power levels calculated using the CadnaA noise model at the reference distance to the noise source. Numbers may vary due to size differences between point and area noise sources.

### 8.2.2 AIR CONDITIONER

To determine the noise levels associated with the Project air conditioner/furnace units, Urban Crossroads collected reference noise level measurements of a similar air conditioner/furnace on a travel trailer. The air conditioner/furnace reference noise level measured 52.1 dBA L<sub>eq</sub> at 50 feet. For this noise analysis, air conditioner activity is expected to operate continuously for 45 minutes per hour during the daytime hours and 30 minutes per hour during the nighttime hours and will be located three feet above the ground elevation.

### 8.2.3 CONTAINER STORAGE ACTIVITY

At a uniform reference distance of 50 feet, Urban Crossroads collected a reference noise level of 71.8 dBA L<sub>eq</sub>. The loading dock activity noise level measurement was taken over a fifteen-minute period and represents multiple noise sources taken from the center of activity. The reference noise level measurement includes employees unloading a docked truck container, including the squeaking of the truck's shocks when weight was removed from the truck, employees playing music over a radio, as well as a forklift horn and backup alarm. In addition, during the noise level measurement, a truck entered the loading dock area and proceeded to reverse and dock in a nearby loading bay, adding truck engine, idling, and air brake noise, in addition to the ongoing idling of an already docked truck. Loading dock activity is estimated during all the daytime, hours.

## 8.3 CADNA A NOISE PREDICTION MODEL

To fully describe the exterior operational noise levels from the Project, Urban Crossroads, Inc. developed a noise prediction model using the CadnaA (Computer Aided Noise Abatement) computer program. CadnaA can analyze multiple types of noise sources using the spatially accurate Project site plan, georeferenced Nearmap aerial imagery, topography, buildings, and barriers in its calculations to predict outdoor noise levels.

Using the ISO 9613-2 protocol, CadnaA will calculate the distance from each noise source to the noise receiver locations, using the ground absorption, distance, and barrier/building attenuation

inputs to provide a summary of noise level at each receiver and the partial noise level contributions by noise source. Consistent with the ISO 9613-2 protocol, the CadnaA noise prediction model relies on the reference sound power level ( $L_w$ ) to describe individual noise sources. While sound pressure levels (e.g.,  $L_{eq}$ ) quantify in decibels the intensity of given sound sources at a reference distance, sound power levels ( $L_w$ ) are connected to the sound source and are independent of distance. Sound pressure levels vary substantially with distance from the source and diminish because of intervening obstacles and barriers, air absorption, wind, and other factors. Sound power is the acoustical energy emitted by the sound source and is an absolute value that is not affected by the environment.

The operational noise level calculations provided in this noise study account for the distance attenuation provided due to geometric spreading, when sound from a localized stationary source (i.e., a point source) propagates uniformly outward in a spherical pattern. A default ground attenuation factor of 0.5 was used in the noise analysis to account for mixed ground representing a combination of hard and soft surfaces. Appendix 8.1 includes the detailed noise model inputs used to estimate the Project operational noise levels presented in this section.

#### 8.4 PROJECT OPERATIONAL NOISE LEVELS

Using the reference noise levels to represent the proposed Project operations that include air conditioning unit, Urban Crossroads, Inc. calculated the operational source noise levels that are expected to be generated at the Project site and the Project-related noise level increases that would be experienced at each of the sensitive receiver locations. Table 8-2 shows the Project operational noise levels during the daytime hours of 7:00 a.m. to 10:00 p.m. The daytime hourly noise levels at the off-site receiver locations are expected to range from 37.9 to 46.8 dBA  $L_{eq}$ .

**TABLE 8-2: DAYTIME PROJECT OPERATIONAL NOISE LEVELS**

Noise Source <sup>1</sup>	Daytime Noise Level (dBA $L_{eq}$ )				
	R1	R2	R3	R4	R5
Air Conditioning	37.9	39.7	41.1	42.7	46.7
Container Storage Activity	15.6	17.5	21.9	23.8	30.3
<b>Total (All Noise Sources)</b>	<b>37.9</b>	<b>39.7</b>	<b>41.2</b>	<b>42.8</b>	<b>46.8</b>

<sup>1</sup> See Exhibit 8-A for the noise source locations. CadnaA noise model calculations are included in Appendix 8.1.

Table 8-3 shows the Project operational noise levels during the nighttime hours of 10:00 p.m. to 7:00 a.m. The nighttime hourly noise levels at the off-site receiver locations are expected to range from 37.9 to 46.8 dBA  $L_{eq}$ . The differences between the daytime and nighttime noise levels are largely related to the duration of noise activity with minimal nighttime operations (Table 8-1).

**TABLE 8-3: NIGHTTIME PROJECT OPERATIONAL NOISE LEVELS**

Noise Source <sup>1</sup>	Nighttime Noise Level (dBA Leq)				
	R1	R2	R3	R4	R5
Air Conditioning	37.9	39.7	41.1	42.7	46.7
Container Storage Activity	12.9	14.7	19.1	21.1	27.6
<b>Total (All Noise Sources)</b>	<b>37.9</b>	<b>39.7</b>	<b>41.1</b>	<b>42.7</b>	<b>46.8</b>

<sup>1</sup> See Exhibit 8-A for the noise source locations. CadnaA noise model calculations are included in Appendix 8.1.

## 8.5 PROJECT OPERATIONAL NOISE LEVEL COMPLIANCE

To demonstrate compliance with local noise regulations, the Project-only operational noise levels are evaluated against exterior noise level thresholds based on the County of San Bernardino exterior noise level standards at the nearest noise-sensitive receiver locations. Table 8-4 shows the operational noise levels associated with the Project will satisfy the County of San Bernardino exterior noise level standards at all nearby receiver locations. Therefore, the operational noise impacts are considered *less than significant* at the nearest noise-sensitive receiver locations.

**TABLE 8-4: OPERATIONAL NOISE LEVEL COMPLIANCE**

Receiver Location <sup>1</sup>	Project Operational Noise Levels (dBA Leq) <sup>2</sup>		Measurement Location	Existing Ambient Noise Levels (dBA Leq)		Exterior Noise Level Standards (dBA Leq) <sup>3</sup>		Noise Level Standards Exceeded? <sup>4</sup>	
	Daytime	Nighttime		Daytime	Nighttime	Daytime	Nighttime	Daytime	Nighttime
R1	37.9	37.9	L1	51.7	43.3	55.0	45.0	No	No
R2	39.7	39.7	L2	52.9	50.3	55.0	50.0	No	No
R3	41.2	41.1	L3	59.0	53.8	59.0	53.0	No	No
R4	42.8	42.7	L4	62.3	58.8	62.0	58.0	No	No
R5	46.8	46.8	L5	69.5	65.0	69.0	65.0	No	No

<sup>1</sup> See Exhibit 6-A for the receiver locations.

<sup>2</sup> Proposed Project operational noise levels as shown in Tables 8-2 and 8-3.

<sup>3</sup> Exterior noise level standards are shown in Table 3-1. Bold numbers indicate the noise limit has been adjusted to match ambient noise level measurements in Table 5-1, which are rounded down to be conservative.

<sup>4</sup> Do the estimated Project operational noise source activities exceed the noise level standards?

"Daytime" = 7:01 a.m. to 10:00 p.m.; "Nighttime" = 10:01 p.m. to 7:00 a.m.

## 8.6 PROJECT OPERATIONAL NOISE LEVEL INCREASES

To describe the Project operational noise level increases, the Project operational noise levels are combined with the existing ambient noise levels measurements for the nearest receiver locations potentially impacted by Project operational noise sources. Since the units used to measure noise, decibels (dB), are logarithmic units, the Project-operational and existing ambient noise levels cannot be combined using standard arithmetic equations. (2) Instead, they must be logarithmically added using the following base equation:

$$SPL_{Total} = 10\log_{10}[10^{SPL1/10} + 10^{SPL2/10} + \dots + 10^{SPLn/10}]$$

Where “SPL1,” “SPL2,” etc. are equal to the sound pressure levels being combined, or in this case, the Project-operational and existing ambient noise levels. The difference between the combined Project and ambient noise levels describes the Project noise level increases to the existing ambient noise environment. As indicated in Tables 8-5 and 8-6, the Project will generate daytime and nighttime operational noise level increases ranging from less than 0.01 to 1.1 dBA  $L_{eq}$  at the nearest receiver locations. Project-related operational noise level increases will satisfy the operational noise level increase significance criteria presented in Table 4-1. Therefore, the incremental Project operational noise level increase is considered *less than significant* at all receiver locations.

**TABLE 8-5: DAYTIME PROJECT OPERATIONAL NOISE LEVEL INCREASES**

Receiver Location <sup>1</sup>	Total Project Operational Noise Level <sup>2</sup>	Measurement Location <sup>3</sup>	Reference Ambient Noise Levels <sup>4</sup>	Combined Project and Ambient <sup>5</sup>	Project Increase <sup>6</sup>	Increase Criteria <sup>7</sup>	Increase Criteria Exceeded?
R1	37.9	L1	51.7	51.9	0.2	5	No
R2	39.7	L2	52.9	53.1	0.2	5	No
R3	41.2	L3	59.0	59.1	0.1	5	No
R4	42.8	L4	62.3	62.3	0.0	3	No
R5	46.8	L4	62.3	62.4	0.1	3	No

<sup>1</sup> See Exhibit 6-A for the receiver locations.

<sup>2</sup> Total Project daytime operational noise levels as shown in Table 8-2.

<sup>3</sup> Reference noise level measurement locations as shown on Exhibit 5-A.

<sup>4</sup> Observed daytime ambient noise levels as shown in Table 5-1.

<sup>5</sup> Represents the combined ambient conditions plus the Project activities.

<sup>6</sup> The noise level increase expected with the addition of the proposed Project activities.

<sup>7</sup> Significance increase criteria as shown in Table 4-1.

TABLE 8-6: NIGHTTIME OPERATIONAL NOISE LEVEL INCREASES

Receiver Location <sup>1</sup>	Total Project Operational Noise Level <sup>2</sup>	Measurement Location <sup>3</sup>	Reference Ambient Noise Levels <sup>4</sup>	Combined Project and Ambient <sup>5</sup>	Project Increase <sup>6</sup>	Increase Criteria <sup>7</sup>	Increase Criteria Exceeded?
R1	37.9	L1	43.3	44.4	1.1	5	No
R2	39.7	L2	50.3	50.7	0.4	5	No
R3	41.1	L3	53.8	54.0	0.2	5	No
R4	42.7	L4	58.8	58.9	0.1	5	No
R5	46.8	L4	58.8	59.1	0.3	5	No

<sup>1</sup> See Exhibit 6-A for the receiver locations.

<sup>2</sup> Total Project nighttime operational noise levels as shown in Table 8-3.

<sup>3</sup> Reference noise level measurement locations as shown on Exhibit 5-A.

<sup>4</sup> Observed nighttime ambient noise levels as shown in Table 5-1.

<sup>5</sup> Represents the combined ambient conditions plus the Project activities.

<sup>6</sup> The noise level increase expected with the addition of the proposed Project activities.

<sup>7</sup> Significance increase criteria as shown in Table 4-1.

## 9 REFERENCES

1. **State of California.** *California Environmental Quality Act, Appendix G.* 2018.
2. **California Department of Transportation Environmental Program.** *Technical Noise Supplement - A Technical Supplement to the Traffic Noise Analysis Protocol.* Sacramento, CA : s.n., September 2013.
3. **Environmental Protection Agency Office of Noise Abatement and Control.** *Information on Levels of Environmental Noise Requisite to Protect Public Health and Welfare with an Adequate Margin of Safety.* March 1974. EPA/ONAC 550/9/74-004.
4. **U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning, Noise and Air Quality Branch.** *Highway Traffic Noise Analysis and Abatement Policy and Guidance.* December 2011.
5. **U.S. Department of Transportation, Federal Highway Administration.** *Highway Traffic Noise in the United States, Problem and Response.* April 2000. p. 3.
6. **U.S. Environmental Protection Agency Office of Noise Abatement and Control.** *Noise Effects Handbook-A Desk Reference to Health and Welfare Effects of Noise.* October 1979 (revised July 1981). EPA 550/9/82/106.
7. **U.S. Department of Transportation, Federal Transit Administration.** *Transit Noise and Vibration Impact Assessment Manual, FTA Report No. 0123.* September 2018.
8. **California Department of Transportation.** *Transportation and Construction Vibration Guidance Manual.* April 2020.
9. **Office of Planning and Research.** *State of California General Plan Guidelines.* October 2017.
10. **San Bernardino County.** *Countywide Plan.* 2023.
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13. **Federal Interagency Committee on Noise.** *Federal Agency Review of Selected Airport Noise Analysis Issues.* August 1992.
14. **U.S. Department of Transportation, Federal Highway Administration, Office of Environment and Planning, Noise and Air Quality Branch.** *Highway Traffic Noise Analysis and Abatement Policy and Guidance.* December 2011.
15. **California Department of Transportation.** *Technical Noise Supplement.* November 2009.
16. **American National Standards Institute (ANSI).** *Specification for Sound Level Meters ANSI S1.4-2014/IEC 61672-1:2013.*
17. **Urban Crossroads.** *Earl Graham (CUP 2022-00082) Trip Generation Assessment.* 2024.
18. **Fehr Peers.** *San Bernardino Countywide Plan, Transportation Existing Conditions Report.* 2018.
19. **Bayerisches Landesamt für Umwelt.** *Parking Area Noise, 6. Revised Edition.* 2007. ISBN 3-936385-26-2, ISSN 0723-0028.
20. *Prediction of parking area noise in Australian conditions.* **Johnson, Laurence Nicol and Paul.** Paper Number 39, s.l. : Gold Coast, Australia, 2-4 November 2011, Vol. Proceedings of ACOUSTICS 2011.

21. **U.S. Department of Transportation, Federal Highway Administration.** *Road Construction Noise Model, version 1.0.* 2006.

## 10 CERTIFICATION

The contents of this noise study report represent an accurate depiction of the noise environment and impacts associated with the proposed Earl Graham Project. The information contained in this noise study report is based on the best available data at the time of preparation. If you have any questions, please contact me directly at (619) 778-1971.

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Senior Associate  
URBAN CROSSROADS, INC.  
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### EDUCATION

Bachelor of Science in Urban and Regional Planning  
California Polytechnic State University, Pomona • June 2000

### PROFESSIONAL AFFILIATIONS

ASA – Acoustical Society of America  
AEP – Association of Environmental Planners  
AWMA – Air and Waste Management Association  
INCE – Institute of Noise Control Engineers - Member

### PROFESSIONAL CERTIFICATIONS

Approved Acoustical Consultant • County of San Diego  
FHWA Traffic Noise Model of Training • November 2004  
CadnaA Basic and Advanced Training Certificate • October 2008

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**APPENDIX 3.1:**

**COUNTY OF SAN BERNARDINO DEVELOPMENT CODE**

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**§ 83.01.080 Noise.**

This Section establishes standards concerning acceptable noise levels for both noise-sensitive land uses and for noise-generating land uses.

(a) *Noise Measurement.* Noise shall be measured:

- (1) At the property line of the nearest site that is occupied by, and/or zoned or designated to allow the development of noise-sensitive land uses;
- (2) With a sound level meter that meets the standards of the American National Standards Institute (ANSI § SI4 1979, Type 1 or Type 2);
- (3) Using the “A” weighted sound pressure level scale in decibels (ref. pressure = 20 micronewtons per meter squared). The unit of measure shall be designated as dB(A).

(b) *Noise Impacted Areas.* Areas within the County shall be designated as “noise-impacted” if exposed to existing or projected future exterior noise levels from mobile or stationary sources exceeding the standards listed in Subdivision (d) (Noise Standards for Stationary Noise Sources) and Subdivision (e) (Noise Standards for Adjacent Mobile Noise Sources), below. New development of residential or other noise-sensitive land uses shall not be allowed in noise-impacted areas unless effective mitigation measures are incorporated into the project design to reduce noise levels to these standards. Noise-sensitive land uses shall include residential uses, schools, hospitals, nursing homes, religious institutions, libraries, and similar uses.

(c) *Noise Standards for Stationary Noise Sources.*

(1) *Noise Standards.* Table 83-2 (Noise Standards for Stationary Noise Sources) describes the noise standard for emanations from a stationary noise source, as it affects adjacent properties:

<b>Table 83-2</b>		
<b>Noise Standards for Stationary Noise Sources</b>		
<b>Affected Land Uses (Receiving Noise)</b>	<b>7:00 a.m. - 10:00 p.m. Leq</b>	<b>10:00 p.m. - 7:00 a.m. Leq</b>

<b>Table 83-2</b>		
<b>Noise Standards for Stationary Noise Sources</b>		
<b>Affected Land Uses (Receiving Noise)</b>	<b>7:00 a.m. - 10:00 p.m. Leq</b>	<b>10:00 p.m. - 7:00 a.m. Leq</b>
Residential	55 dB(A)	45 dB(A)
Professional Services	55 dB(A)	55 dB(A)
Other Commercial	60 dB(A)	60 dB(A)
Industrial	70 dB(A)	70 dB(A)

Leq = (Equivalent Energy Level). The sound level corresponding to a steady-state sound level containing the same total energy as a time-varying signal over a given sample period, typically one, eight or 24 hours.

dB(A) = (A-weighted Sound Pressure Level). The sound pressure level, in decibels, as measured on a sound level meter using the A-weighting filter network. The A-weighting filter de-emphasizes the very low and very high frequency components of the sound, placing greater emphasis on those frequencies within the sensitivity range of the human ear.

Ldn = (Day-Night Noise Level). The average equivalent A-weighted sound level during a 24-hour day obtained by adding 10 decibels to the hourly noise levels measured during the night (from 10:00 p.m. to 7:00 a.m.). In this way Ldn takes into account the lower tolerance of people for noise during nighttime periods.

(2) *Noise Limit Categories.* No person shall operate or cause to be operated a source of sound at a location or allow the creation of noise on property owned, leased, occupied, or otherwise controlled by the person, which causes the noise level, when measured on another property, either incorporated or unincorporated, to exceed any one of the following:

- (A) The noise standard for the receiving land use as specified in Subdivision (b) (Noise-Impacted Areas), above, for a cumulative period of more than 30 minutes in any hour.
- (B) The noise standard plus five dB(A) for a cumulative period of more than 15 minutes in any hour.
- (C) The noise standard plus ten dB(A) for a cumulative period of more than five minutes in any hour.
- (D) The noise standard plus 15 dB(A) for a cumulative period of more than one minute in any hour.
- (E) The noise standard plus 20 dB(A) for any period of time.

(d) *Noise Standards for Adjacent Mobile Noise Sources.* Noise from mobile sources may affect adjacent properties adversely. When it does, the noise shall be mitigated for any new development to a level that shall not exceed the standards described in the following Table 83-3 (Noise Standards for Adjacent Mobile Noise Sources).

<b>Table 83-3</b>			
<b>Noise Standards for Adjacent Mobile Noise Sources</b>			
<b>Land Use</b>		<b>Ldn (or CNEL) dB(A)</b>	
<b>Categories</b>	<b>Uses</b>	<b>Interior <sup>(1)</sup></b>	<b>Exterior <sup>(2)</sup></b>

<b>Table 83-3</b>			
<b>Noise Standards for Adjacent Mobile Noise Sources</b>			
<b>Land Use</b>		<b>Ldn (or CNEL) dB(A)</b>	
<b>Categories</b>	<b>Uses</b>	<b>Interior <sup>(1)</sup></b>	<b>Exterior <sup>(2)</sup></b>
Residential	Single and multi-family, duplex, mobile homes	45	60 <sup>(3)</sup>
Commercial	Hotel, motel, transient housing	45	60 <sup>(3)</sup>
	Commercial retail, bank, restaurant	50	N/A
	Office building, research and development, professional offices	45	65
	Amphitheater, concert hall, auditorium, movie theater	45	N/A
Institutional/Public	Hospital, nursing home, school classroom, religious institution, library	45	65
Open Space	Park	N/A	65

**Notes:**

(1) The indoor environment shall exclude bathrooms, kitchens, toilets, closets and corridors.

(2) The outdoor environment shall be limited to:

- Hospital/office building patios
- Hotel and motel recreation areas
- Mobile home parks
- Multi-family private patios or balconies

- Park picnic areas
- Private yard of single-family dwellings
- School playgrounds

(3) An exterior noise level of up to 65 dB(A) (or CNEL) shall be allowed provided exterior noise levels have been substantially mitigated through a reasonable application of the best available noise reduction technology, and interior noise exposure does not exceed 45 dB(A) (or CNEL) with windows and doors closed. Requiring that windows and doors remain closed to achieve an acceptable interior noise level shall necessitate the use of air conditioning or mechanical ventilation.

CNEL = (Community Noise Equivalent Level). The average equivalent A-weighted sound level during a 24-hour day, obtained after addition of approximately five decibels to sound levels in the evening from 7:00 p.m. to 10:00 p.m. and ten decibels to sound levels in the night from 10:00 p.m. to 7:00 a.m.

(e) *Increases in Allowable Noise Levels.* If the measured ambient level exceeds any of the first four noise limit categories in Subdivision (d)(2), above, the allowable noise exposure standard shall be increased to reflect the ambient noise level. If the ambient noise level exceeds the fifth noise limit category in Subdivision (d)(2), above, the maximum allowable noise level under this category shall be increased to reflect the maximum ambient noise level.

(f) *Reductions in Allowable Noise Levels.* If the alleged offense consists entirely of impact noise or simple tone noise, each of the noise levels in Table 83-2 (Noise Standards for Stationary Noise Sources) shall be reduced by five dB(A).

(g) *Exempt Noise.* The following sources of noise shall be exempt from the regulations of this Section:

- (1) Motor vehicles not under the control of the commercial or industrial use.
- (2) Emergency equipment, vehicles, and devices.
- (3) Temporary construction, maintenance, repair, or demolition activities between 7:00 a.m. and 7:00 p.m., except Sundays and Federal holidays.

(h) *Noise Standards for Other Structures.* All other structures shall be sound attenuated against the combined input of all present and projected exterior noise to not exceed the criteria.

**Table 83-4**

**Noise Standards for Other Structures**

<b>Typical Uses</b>	<b>12-Hour Equivalent Sound Level (Interior) in dBA Ldn</b>
Educational, institutions, libraries, meeting facilities, etc.	45
General office, reception, etc.	50
Retail stores, restaurants, etc.	55
Other areas for manufacturing, assembly, testing, warehousing, etc.	65

In addition, the average of the maximum levels on the loudest of intrusive sounds occurring during a 24-hour period shall not exceed 65 dBA interior.

(Ord. 4011, passed - -2007; Am. Ord. 4245, passed - -2014)

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**APPENDIX 5.1:**  
**STUDY AREA PHOTOS**

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16122 - Earl Graham

16122\_L1\_A 1.North  
34, 25' 14.900000",117, 12' 46.050000"



16122\_L1\_A 2.South  
34, 25' 14.860000",117, 12' 46.050000"



16122\_L1\_A 3.East  
34, 25' 14.660000",117, 12' 46.020000"



16122\_L1\_A 4.West  
34, 25' 14.660000",117, 12' 46.020000"



16122 - Earl Graham

16122\_L2\_B 1.North  
34, 24' 58.380000",117, 12' 56.760000"



16122\_L2\_B 2.South  
34, 24' 58.360000",117, 12' 56.820000"



16122\_L2\_B 3.East  
34, 24' 58.330000",117, 12' 56.570000"



16122\_L2\_B 4.West  
34, 24' 58.340000",117, 12' 56.730000"



16122 - Earl Graham

16122\_L3\_C 1.North  
34, 25' 1.130000", 117, 13' 28.350000"



16122\_L3\_C 2.South  
34, 25' 1.050000", 117, 13' 28.460000"



16122\_L3\_C 3.East  
34, 25' 1.030000", 117, 13' 28.430000"



16122\_L3\_C 4.West  
34, 25' 1.060000", 117, 13' 28.460000"



16122 - Earl Graham

16122\_L4\_D 1.North  
34, 25' 6.870000", 117, 13' 29.940000"



16122\_L4\_D 2.South  
34, 25' 6.640000", 117, 13' 29.880000"



16122\_L5\_E 1.North  
34, 25' 11.420000", 117, 13' 29.170000"



16122\_L5\_E 2.South  
34, 25' 11.180000", 117, 13' 29.200000"



16122 - Earl Graham

16122\_L5\_E 3.East

34, 25' 11.210000",117, 13' 29.230000"



16122\_L5\_E 4.West

34, 25' 11.280000",117, 13' 29.250000"



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**APPENDIX 5.2:**  
**NOISE LEVEL MEASUREMENT WORKSHEETS**

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## 24-Hour Noise Level Measurement Summary

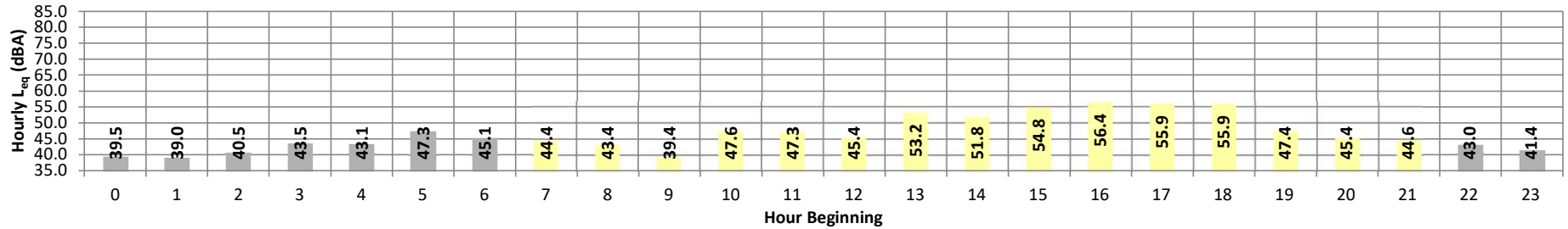
Date: Wednesday, July 24, 2024  
Project: Ear Graham Project

Location: L1 - Located northeast of the site near the residence at 9426  
Source: Iroquois Ave.

Meter: Piccolo II

JN: 16122  
Analyst: Z. Ibrahim

Hourly  $L_{eq}$  dBA Readings (unadjusted)



Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	$L_{eq}$	Adj.	Adj. $L_{eq}$
Night	0	39.5	45.4	34.9	44.9	44.5	43.5	42.8	40.3	38.2	35.8	35.4	35.0	39.5	10.0	49.5
	1	39.0	44.4	34.5	44.0	43.5	42.6	41.9	40.0	37.8	35.6	35.2	34.7	39.0	10.0	49.0
	2	40.5	49.7	34.6	49.3	48.1	45.9	44.3	40.4	38.4	35.6	35.1	34.8	40.5	10.0	50.5
	3	43.5	53.6	35.0	53.3	52.7	50.5	47.9	42.8	39.6	36.3	35.6	35.1	43.5	10.0	53.5
	4	43.1	49.4	37.7	49.2	48.7	47.5	46.3	43.7	42.1	39.1	38.5	37.9	43.1	10.0	53.1
	5	47.3	53.3	41.6	53.0	52.6	51.5	50.7	48.2	46.1	42.8	42.3	41.7	47.3	10.0	57.3
Day	6	45.1	50.2	41.3	49.6	49.2	48.3	47.7	46.0	44.5	42.2	41.9	41.4	45.1	10.0	55.1
	7	44.4	54.0	38.5	53.6	53.2	51.4	49.4	42.9	41.0	39.2	39.0	38.6	44.4	0.0	44.4
	8	43.4	55.2	36.1	54.7	54.1	50.7	47.8	40.3	38.1	36.7	36.5	36.2	43.4	0.0	43.4
	9	39.4	48.2	33.3	47.8	47.3	45.7	44.4	38.9	35.9	33.9	33.7	33.4	39.4	0.0	39.4
	10	47.6	60.2	33.2	59.9	59.1	55.8	52.4	42.3	36.6	33.9	33.7	33.3	47.6	0.0	47.6
	11	47.3	60.8	34.6	60.1	59.2	55.3	51.6	39.5	37.0	35.2	35.0	34.7	47.3	0.0	47.3
	12	45.4	54.8	37.3	54.3	53.7	52.1	50.3	44.7	42.1	38.7	38.1	37.5	45.4	0.0	45.4
	13	53.2	64.6	40.8	64.2	63.4	60.5	57.9	51.4	47.9	42.8	41.9	41.0	53.2	0.0	53.2
	14	51.8	60.7	42.6	60.2	59.5	57.9	56.4	52.0	48.9	44.3	43.6	42.9	51.8	0.0	51.8
	15	54.8	65.2	43.7	64.4	63.6	61.0	58.9	54.9	51.2	46.0	45.1	44.0	54.8	0.0	54.8
	16	56.4	65.6	45.3	64.9	64.1	62.5	61.0	56.8	53.3	48.1	47.0	45.7	56.4	0.0	56.4
	17	55.9	64.7	45.1	64.0	63.3	61.7	60.5	56.5	53.2	47.4	46.5	45.5	55.9	0.0	55.9
	18	55.9	68.0	42.1	67.5	66.8	64.5	61.9	50.0	47.6	44.0	43.3	42.4	55.9	0.0	55.9
	19	47.4	54.4	41.2	53.8	53.1	51.8	50.9	48.1	46.1	42.7	42.1	41.4	47.4	5.0	52.4
	20	45.4	51.9	39.9	51.3	50.8	49.7	48.9	46.0	44.2	41.3	40.8	40.1	45.4	5.0	50.4
	21	44.6	52.9	39.3	52.5	51.8	49.6	47.9	44.9	42.9	40.4	40.0	39.5	44.6	5.0	49.6
Night	22	43.0	49.3	36.8	48.9	48.5	47.6	46.7	43.9	41.6	38.3	37.6	37.0	43.0	10.0	53.0
Night	23	41.4	48.0	35.1	47.5	46.8	45.7	45.1	42.6	39.9	36.4	35.8	35.3	41.4	10.0	51.4
Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	24-Hour CNEL Leq (dBA)		
Day	Min	39.4	48.2	33.2	47.8	47.3	45.7	44.4	38.9	35.9	33.9	33.7	33.3	52.6	51.7	43.3
	Max	56.4	68.0	45.3	67.5	66.8	64.5	61.9	56.8	53.3	48.1	47.0	45.7			
Energy Average		51.7	Average:		58.2	57.5	55.4	53.4	47.3	44.4	41.0	40.4	39.7			
Night	Min	39.0	44.4	34.5	44.0	43.5	42.6	41.9	40.0	37.8	35.6	35.1	34.7			
	Max	47.3	53.6	41.6	53.3	52.7	51.5	50.7	48.2	46.1	42.8	42.3	41.7			
Energy Average		43.3	Average:		48.8	48.3	47.0	45.9	43.1	40.9	38.0	37.5	37.0			

### 24-Hour Noise Level Measurement Summary

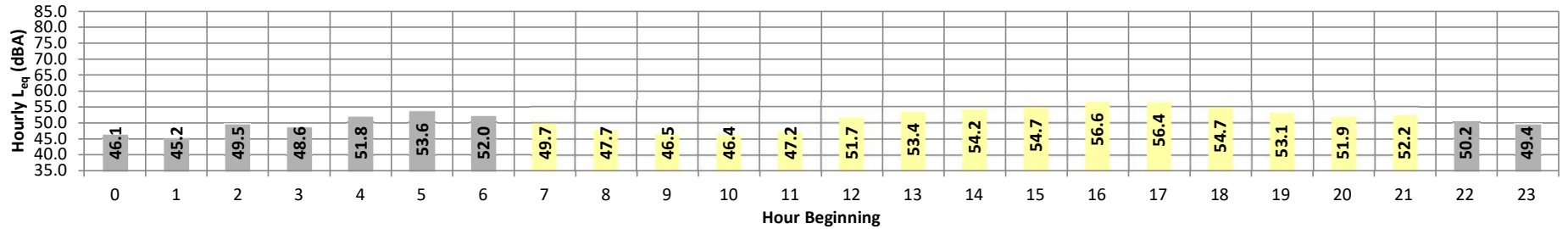
Date: Wednesday, July 24, 2024  
Project: Ear Graham Project

Location: L2 - Located southeast of the site near the residence at 20535  
Source: Rock Springs Rd.

Meter: Piccolo II

JN: 16122  
Analyst: Z. Ibrahim

Hourly  $L_{eq}$  dBA Readings (unadjusted)



Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	$L_{eq}$	Adj.	Adj. $L_{eq}$
Night	0	46.1	53.5	35.7	53.2	52.8	51.7	50.9	47.3	43.4	37.0	36.4	35.8	46.1	10.0	56.1
	1	45.2	53.8	34.9	53.4	53.1	51.3	50.2	45.9	41.5	36.7	35.9	35.1	45.2	10.0	55.2
	2	49.5	60.8	36.0	59.9	58.9	56.5	54.7	48.7	43.3	37.9	37.2	36.2	49.5	10.0	59.5
	3	48.6	56.3	37.9	55.9	55.3	54.3	53.3	49.7	46.1	40.3	39.0	38.1	48.6	10.0	58.6
	4	51.8	58.7	42.6	58.4	58.0	56.9	56.2	53.2	49.7	44.3	43.7	42.9	51.8	10.0	61.8
	5	53.6	58.9	46.3	58.7	58.4	57.8	57.2	54.8	52.4	48.3	47.5	46.6	53.6	10.0	63.6
	6	52.0	57.3	46.4	57.1	56.8	55.8	55.2	53.0	51.1	47.8	47.2	46.6	52.0	10.0	62.0
Day	7	49.7	55.8	43.7	55.6	55.3	54.2	53.3	50.6	48.3	45.1	44.4	43.9	49.7	0.0	49.7
	8	47.7	53.3	41.5	53.1	52.7	51.9	51.4	48.6	46.5	43.1	42.4	41.7	47.7	0.0	47.7
	9	46.5	52.1	39.7	51.8	51.5	50.8	50.3	47.5	45.1	41.5	40.7	39.9	46.5	0.0	46.5
	10	46.4	52.1	39.2	51.8	51.5	50.9	50.3	47.4	44.7	40.8	40.0	39.3	46.4	0.0	46.4
	11	47.2	54.3	40.0	54.0	53.5	52.3	51.5	47.9	45.3	41.6	41.0	40.2	47.2	0.0	47.2
	12	51.7	60.9	42.6	60.2	59.4	57.4	56.1	51.9	49.1	44.7	43.9	43.0	51.7	0.0	51.7
	13	53.4	62.1	44.5	61.6	61.1	58.8	57.4	53.8	51.2	46.9	45.9	44.8	53.4	0.0	53.4
	14	54.2	61.6	45.2	61.2	60.6	59.2	58.2	55.0	52.5	48.0	46.9	45.6	54.2	0.0	54.2
	15	54.7	63.1	45.7	62.4	61.7	60.1	58.9	55.4	52.5	48.0	47.1	46.0	54.7	0.0	54.7
	16	56.6	65.2	47.3	64.4	63.5	61.6	60.5	57.3	54.6	50.1	49.0	47.7	56.6	0.0	56.6
	17	56.4	64.3	48.6	63.6	62.9	61.0	60.0	57.2	55.0	50.8	49.9	48.9	56.4	0.0	56.4
	18	54.7	60.6	46.5	60.2	59.8	58.8	58.2	55.9	53.6	48.9	47.9	46.8	54.7	0.0	54.7
	19	53.1	59.0	45.0	58.6	58.3	57.5	56.9	54.2	51.7	47.2	46.3	45.3	53.1	5.0	58.1
	20	51.9	58.1	43.5	57.8	57.5	56.5	55.8	53.2	50.3	45.5	44.6	43.7	51.9	5.0	56.9
	21	52.2	58.3	43.0	58.0	57.6	56.8	56.2	53.7	50.8	45.3	44.3	43.3	52.2	5.0	57.2
Night	22	50.2	56.3	40.6	56.0	55.7	54.9	54.2	51.8	48.6	42.9	41.9	40.8	50.2	10.0	60.2
	23	49.4	58.5	37.3	58.1	57.5	55.7	54.5	49.8	45.4	39.8	38.9	37.6	49.4	10.0	59.4
Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	24-Hour CNEL Leq (dBA)		
Day	Min	46.4	52.1	39.2	51.8	51.5	50.8	50.3	47.4	44.7	40.8	40.0	39.3	57.6	52.9	50.3
	Max	56.6	65.2	48.6	64.4	63.5	61.6	60.5	57.3	55.0	50.8	49.9	48.9			
Energy Average		52.9	Average:		58.3	57.8	56.5	55.7	52.6	50.1	45.8	45.0	44.0			
Night	Min	45.2	53.5	34.9	53.2	52.8	51.3	50.2	45.9	41.5	36.7	35.9	35.1			
	Max	53.6	60.8	46.4	59.9	58.9	57.8	57.2	54.8	52.4	48.3	47.5	46.6			
Energy Average		50.3	Average:		56.8	56.3	55.0	54.1	50.5	46.8	41.7	40.8	40.0			

## 24-Hour Noise Level Measurement Summary

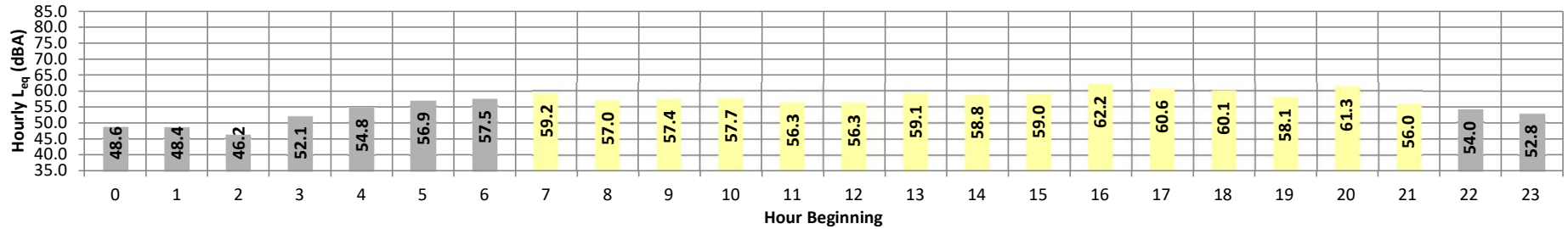
Date: Wednesday, July 24, 2024  
Project: Ear Graham Project

Location: L3 - Located west of the site near the residence at 9141 Deep  
Source: Creek Rd.

Meter: Piccolo II

JN: 16122  
Analyst: Z. Ibrahim

Hourly  $L_{eq}$  dBA Readings (unadjusted)



Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	$L_{eq}$	Adj.	Adj. $L_{eq}$
Night	0	48.6	60.1	36.7	59.6	58.6	55.8	53.5	46.5	41.9	38.0	37.4	36.8	48.6	10.0	58.6
	1	48.4	61.9	34.3	61.2	60.3	55.3	52.2	43.8	39.3	35.6	35.0	34.5	48.4	10.0	58.4
	2	46.2	58.5	34.6	57.6	56.5	53.6	51.3	44.0	38.6	35.7	35.2	34.8	46.2	10.0	56.2
	3	52.1	63.3	37.7	62.8	62.0	59.9	58.0	50.2	45.5	39.2	38.5	37.9	52.1	10.0	62.1
	4	54.8	65.7	42.5	65.1	64.4	62.0	60.1	53.7	49.0	44.0	43.2	42.6	54.8	10.0	64.8
	5	56.9	67.4	46.0	66.9	66.2	63.8	62.0	56.1	51.6	47.4	46.8	46.1	56.9	10.0	66.9
Day	6	57.5	68.1	43.8	67.6	67.0	64.6	62.7	56.8	51.2	45.4	44.7	44.0	57.5	10.0	67.5
	7	59.2	70.3	43.3	69.7	68.8	66.2	64.7	58.8	52.9	44.7	44.0	43.4	59.2	0.0	59.2
	8	57.0	67.0	40.1	66.6	65.9	63.9	62.3	57.4	51.2	42.1	41.0	40.3	57.0	0.0	57.0
	9	57.4	67.8	39.6	67.3	66.6	64.2	62.6	57.6	51.4	41.7	40.8	39.9	57.4	0.0	57.4
	10	57.7	69.2	38.7	68.7	67.9	64.9	62.4	57.0	50.3	41.4	40.2	39.0	57.7	0.0	57.7
	11	56.3	66.0	40.7	65.6	65.0	63.0	61.5	56.8	51.5	42.8	41.9	40.9	56.3	0.0	56.3
	12	56.3	66.6	41.8	66.2	65.4	62.9	61.3	56.6	50.9	43.3	42.7	42.0	56.3	0.0	56.3
	13	59.1	70.4	45.3	69.7	68.8	65.8	64.0	58.5	54.1	47.2	46.4	45.5	59.1	0.0	59.1
	14	58.8	68.0	47.0	67.6	66.9	64.6	63.2	59.4	55.7	49.2	48.2	47.2	58.8	0.0	58.8
	15	59.0	67.7	49.0	67.1	66.4	64.5	63.2	59.9	56.6	50.9	50.1	49.2	59.0	0.0	59.0
	16	62.2	72.0	51.0	71.6	70.9	67.9	66.3	62.5	59.3	53.3	52.3	51.3	62.2	0.0	62.2
	17	60.6	70.0	49.7	69.4	68.6	66.2	64.7	61.3	57.8	51.8	50.8	49.9	60.6	0.0	60.6
	18	60.1	71.2	48.4	70.7	69.5	66.1	64.1	59.9	56.1	50.4	49.4	48.6	60.1	0.0	60.1
	19	58.1	67.4	47.2	67.0	66.4	64.4	63.0	58.4	54.0	48.8	48.2	47.4	58.1	5.0	63.1
	20	61.3	74.3	45.6	74.1	73.0	68.4	65.2	58.0	53.5	47.4	46.6	45.8	61.3	5.0	66.3
21	56.0	67.2	43.1	66.5	65.5	63.1	61.0	55.1	50.3	44.7	44.0	43.2	56.0	5.0	61.0	
Night	22	54.0	64.7	42.4	64.3	63.6	61.4	59.4	52.9	47.8	43.6	43.0	42.5	54.0	10.0	64.0
	23	52.8	64.5	39.0	64.0	63.3	60.5	58.0	50.3	44.7	40.6	39.9	39.1	52.8	10.0	62.8
Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	24-Hour CNEL Leq (dBA)		
Day	Min	56.0	66.0	38.7	65.6	65.0	62.9	61.0	55.1	50.3	41.4	40.2	39.0	62.0	59.0	53.8
	Max	62.2	74.3	51.0	74.1	73.0	68.4	66.3	62.5	59.3	53.3	52.3	51.3			
Energy Average		59.0	Average:		68.5	67.7	65.1	63.3	58.5	53.7	46.7	45.8	44.9			
Night	Min	46.2	58.5	34.3	57.6	56.5	53.6	51.3	43.8	38.6	35.6	35.0	34.5			
	Max	57.5	68.1	46.0	67.6	67.0	64.6	62.7	56.8	51.6	47.4	46.8	46.1			
Energy Average		53.8	Average:		63.2	62.4	59.7	57.5	50.5	45.5	41.1	40.4	39.8			

## 24-Hour Noise Level Measurement Summary

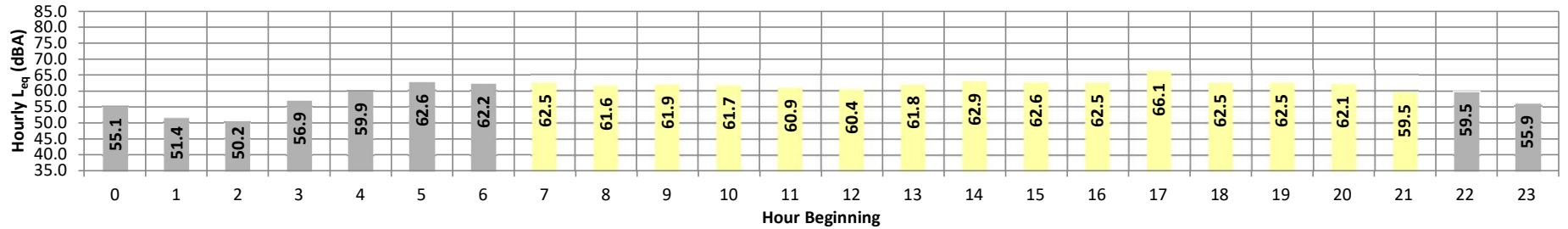
Date: Wednesday, July 24, 2024  
Project: Ear Graham Project

Location: L4 - Located west of the site near the residence at 20276  
Source: Outpost Rd.

Meter: Piccolo II

JN: 16122  
Analyst: Z. Ibrahim

Hourly  $L_{eq}$  dBA Readings (unadjusted)



Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	$L_{eq}$	Adj.	Adj. $L_{eq}$
Night	0	55.1	67.6	41.2	67.3	66.7	63.3	59.8	50.0	45.0	41.6	41.4	41.2	55.1	10.0	65.1
	1	51.4	62.9	40.4	62.7	62.3	59.7	56.6	47.5	42.7	40.6	40.5	40.4	51.4	10.0	61.4
	2	50.2	61.8	40.4	61.5	61.1	58.6	56.0	45.4	41.9	40.5	40.4	40.3	50.2	10.0	60.2
	3	56.9	67.8	41.4	67.6	67.1	65.1	62.6	54.6	47.6	42.1	41.8	41.4	56.9	10.0	66.9
	4	59.9	70.6	43.0	70.3	69.9	67.8	65.8	58.5	51.2	43.8	43.4	43.0	59.9	10.0	69.9
	5	62.6	74.5	46.2	74.2	73.3	70.0	67.1	61.0	61.0	55.1	47.6	46.9	46.3	62.6	10.0
Day	6	62.2	71.8	45.1	71.6	71.2	69.3	67.5	62.5	55.9	47.1	46.1	45.3	62.2	10.0	72.2
	7	62.5	72.2	44.7	72.0	71.5	69.6	67.9	62.7	56.2	46.1	45.2	44.8	62.5	0.0	62.5
	8	61.6	71.4	43.4	71.0	70.6	68.5	66.6	62.0	56.0	44.9	44.0	43.5	61.6	0.0	61.6
	9	61.9	71.2	43.3	71.0	70.6	68.9	67.2	62.6	56.1	45.0	44.0	43.3	61.9	0.0	61.9
	10	61.7	72.1	42.1	71.9	71.5	69.2	66.7	61.4	54.7	43.2	42.4	42.1	61.7	0.0	61.7
	11	60.9	69.9	42.9	69.7	69.2	67.4	66.0	61.9	56.0	44.3	43.6	43.0	60.9	0.0	60.9
	12	60.4	69.6	46.0	69.3	68.9	66.9	65.2	61.1	56.2	48.3	47.3	46.2	60.4	0.0	60.4
	13	61.8	71.3	47.4	71.0	70.6	68.5	66.9	62.2	57.5	49.4	48.4	47.5	61.8	0.0	61.8
	14	62.9	72.8	49.9	72.4	71.8	69.3	67.6	63.2	58.8	52.6	51.5	50.1	62.9	0.0	62.9
	15	62.6	70.9	51.0	70.6	70.3	68.5	67.1	63.3	59.7	53.2	52.2	51.2	62.6	0.0	62.6
	16	62.5	70.8	49.8	70.5	70.0	68.4	67.3	63.5	59.6	52.1	51.1	50.0	62.5	0.0	62.5
	17	66.1	78.7	51.0	78.2	76.9	72.9	69.8	64.4	60.5	53.4	52.1	51.2	66.1	0.0	66.1
	18	62.5	71.3	48.6	71.1	70.7	68.9	67.4	63.2	58.3	50.6	49.5	48.8	62.5	0.0	62.5
	19	62.5	71.5	47.2	71.3	71.0	69.2	67.5	63.2	57.8	49.6	48.5	47.4	62.5	5.0	67.5
	20	62.1	71.3	47.0	71.0	70.6	68.8	67.2	62.8	56.9	49.2	48.1	47.1	62.1	5.0	67.1
21	59.5	69.3	43.6	69.0	68.6	66.7	64.9	59.4	53.0	45.2	44.2	43.7	59.5	5.0	64.5	
Night	22	59.5	71.1	42.6	70.7	70.0	67.2	64.9	57.4	49.8	43.5	43.0	42.6	59.5	10.0	69.5
Night	23	55.9	66.7	42.0	66.5	66.1	63.9	61.2	54.0	47.5	42.6	42.3	42.0	55.9	10.0	65.9
Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	24-Hour CNEL Leq (dBA)		
Day	Min	59.5	69.3	42.1	69.0	68.6	66.7	64.9	59.4	53.0	43.2	42.4	42.1	66.3	62.3	58.8
	Max	66.1	78.7	51.0	78.2	76.9	72.9	69.8	64.4	60.5	53.4	52.2	51.2			
Energy Average		62.3	Average:		71.3	70.9	68.8	67.0	62.5	57.2	48.5	47.5	46.7			
Night	Min	50.2	61.8	40.4	61.5	61.1	58.6	56.0	45.4	41.9	40.5	40.4	40.3			
	Max	62.6	74.5	46.2	74.2	73.3	70.0	67.5	62.5	55.9	47.6	46.9	46.3			
Energy Average		58.8	Average:		68.0	67.5	65.0	62.4	54.5	48.5	43.3	42.9	42.5			

## 24-Hour Noise Level Measurement Summary

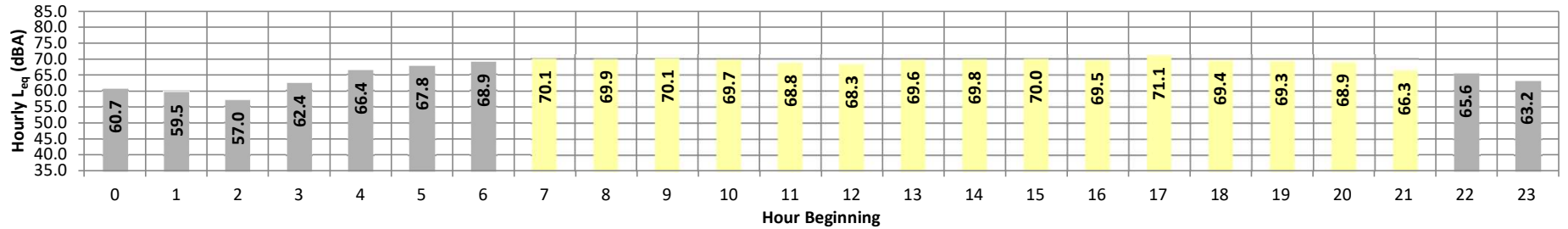
Date: Wednesday, July 24, 2024  
Project: Ear Graham Project

Location: L5 - Located west of the site near the residence at 9293 Deep  
Source: Creek Rd

Meter: Piccolo II

JN: 16122  
Analyst: Z. Ibrahim

Hourly  $L_{eq}$  dBA Readings (unadjusted)



Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	$L_{eq}$	Adj.	Adj. $L_{eq}$
Night	0	60.7	73.7	44.1	73.2	72.2	68.5	65.6	55.0	47.9	44.7	44.5	44.3	60.7	10.0	70.7
	1	59.5	73.4	43.9	72.9	72.0	67.6	63.3	49.7	45.8	44.6	44.4	44.1	59.5	10.0	69.5
	2	57.0	70.5	41.1	70.2	69.3	65.5	61.1	47.0	42.8	41.5	41.3	41.2	57.0	10.0	67.0
	3	62.4	74.9	43.5	74.5	73.7	70.5	67.8	57.4	49.0	44.4	44.0	43.6	62.4	10.0	72.4
	4	66.4	78.4	45.4	77.9	77.0	74.3	72.4	63.3	53.6	46.3	45.9	45.5	66.4	10.0	76.4
	5	67.8	79.3	48.3	78.9	78.2	75.4	73.4	66.4	57.8	49.6	49.0	48.5	67.8	10.0	77.8
Day	6	68.9	79.8	46.6	79.4	78.5	76.1	74.8	68.3	59.8	49.1	47.7	46.8	68.9	10.0	78.9
	7	70.1	80.4	47.7	80.0	79.2	76.8	75.6	70.4	62.5	49.9	48.7	47.8	70.1	0.0	70.1
	8	69.9	80.0	48.3	79.6	78.8	76.5	75.2	70.6	62.6	50.6	49.1	48.4	69.9	0.0	69.9
	9	70.1	80.2	48.2	79.7	78.9	76.7	75.6	70.8	63.2	50.8	49.5	48.4	70.1	0.0	70.1
	10	69.7	80.6	46.2	80.2	79.4	76.6	74.7	69.8	62.6	49.4	47.8	46.5	69.7	0.0	69.7
	11	68.8	78.2	46.9	77.7	77.0	75.3	74.1	70.0	63.2	50.1	48.5	47.2	68.8	0.0	68.8
	12	68.3	77.9	50.6	77.3	76.6	74.7	73.6	69.2	62.6	53.1	51.8	50.8	68.3	0.0	68.3
	13	69.6	80.3	50.9	79.7	78.8	76.1	74.7	70.4	63.0	53.0	51.9	51.1	69.6	0.0	69.6
	14	69.8	79.3	52.3	78.9	78.1	76.0	74.9	71.0	64.3	54.9	53.6	52.5	69.8	0.0	69.8
	15	70.0	79.4	52.6	79.0	78.3	76.2	75.0	71.0	65.3	55.3	53.9	52.7	70.0	0.0	70.0
	16	69.5	78.8	52.7	78.5	77.7	75.7	74.7	70.7	64.5	55.2	54.0	52.9	69.5	0.0	69.5
	17	71.1	81.8	53.1	81.4	80.5	77.5	75.5	71.6	66.0	55.4	54.2	53.2	71.1	0.0	71.1
	18	69.4	79.8	49.1	79.3	78.5	76.0	74.7	70.0	62.2	51.1	50.3	49.3	69.4	0.0	69.4
	19	69.3	79.7	48.9	79.3	78.6	76.2	74.6	69.6	61.3	50.8	49.7	49.0	69.3	5.0	74.3
	20	68.9	79.8	47.5	79.3	78.4	75.8	74.2	69.0	61.2	49.3	48.4	47.6	68.9	5.0	73.9
21	66.3	77.2	45.5	76.7	75.9	73.7	72.2	65.5	56.9	47.0	46.3	45.7	66.3	5.0	71.3	
Night	22	65.6	77.5	44.0	77.0	76.1	73.4	71.5	62.9	52.1	45.0	44.5	44.1	65.6	10.0	75.6
Night	23	63.2	75.6	43.6	75.1	74.2	71.1	68.7	59.5	49.4	44.3	44.0	43.7	63.2	10.0	73.2
Timeframe	Hour	$L_{eq}$	$L_{max}$	$L_{min}$	L1%	L2%	L5%	L8%	L25%	L50%	L90%	L95%	L99%	24-Hour CNEL		
Day	Min	66.3	77.2	45.5	76.7	75.9	73.7	72.2	65.5	56.9	47.0	46.3	45.7	72.8	69.5	65.0
	Max	71.1	81.8	53.1	81.4	80.5	77.5	75.6	71.6	66.0	55.4	54.2	53.2			
Energy Average		69.5	Average:		79.1	78.3	76.0	74.6	70.0	62.8	51.7	50.5	49.5			
Night	Min	57.0	70.5	41.1	70.2	69.3	65.5	61.1	47.0	42.8	41.5	41.3	41.2			
	Max	68.9	79.8	48.3	79.4	78.5	76.1	74.8	68.3	59.8	49.6	49.0	48.5			
Energy Average		65.0	Average:		75.5	74.6	71.4	68.7	58.8	50.9	45.5	45.0	44.6			

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**APPENDIX 8.1:**  
**CADNAA OPERATIONAL NOISE MODEL INPUTS**

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# 12975 - Earl Gram Storage

CadnaA Noise Prediction Model: 16122-02\_Operation.cna

Date: 30.10.24

Analyst: B. Maddux

## Calculation Configuration

Configuration	
Parameter	Value
<b>General</b>	
Max. Error (dB)	0.00
Max. Search Radius #(Unit,LEN)	2000.01
Min. Dist Src to Rcvr	0.00
Partition	
Raster Factor	0.50
Max. Length of Section #(Unit,LEN)	999.99
Min. Length of Section #(Unit,LEN)	1.01
Min. Length of Section (%)	0.00
Proj. Line Sources	On
Proj. Area Sources	On
Ref. Time	
Daytime Penalty (dB)	0.00
Recr. Time Penalty (dB)	5.00
Night-time Penalty (dB)	10.00
DTM	
Standard Height (m)	0.00
Model of Terrain	Triangulation
<b>Reflection</b>	
max. Order of Reflection	2
Search Radius Src	100.00
Search Radius Rcvr	100.00
Max. Distance Source - Rcvr	1000.00 1000.00
Min. Distance Rcvr - Reflector	1.00 1.00
Min. Distance Source - Reflector	0.10
Industrial (ISO 9613)	
Lateral Diffraction	some Obj
Obst. within Area Src do not shield	On
Screening	Incl. Ground Att. over Barrier Dz with limit (20/25)
Barrier Coefficients C1,2,3	3.0 20.0 0.0
Temperature #(Unit,TEMP)	10
rel. Humidity (%)	70
Ground Absorption G	0.50
Wind Speed for Dir. #(Unit,SPEED)	3.0
Roads (TNM)	
Railways (FTA/FRA)	
Aircraft (???)	
Strictly acc. to AzB	

## Receiver Noise Levels

Name	M.	ID	Level Lr			Limit. Value			Land Use			Height (ft)	Coordinates		
			Day (dBA)	Night (dBA)	CNEL (dBA)	Day (dBA)	Night (dBA)	CNEL (dBA)	Type	Auto	Noise Type		X (ft)	Y (ft)	Z (ft)
R1		R1	46.8	12.9	43.8	0.0	0.0	0.0	x	Total	5.00	r	6798869.06	1976989.03	5.00
R2		R2	48.6	14.7	45.6	0.0	0.0	0.0	x	Total	5.00	r	6798653.63	1974925.44	5.00
R3		R3	50.0	19.1	47.0	0.0	0.0	0.0	x	Total	5.00	r	6795606.58	1976208.17	5.00
R4		R4	51.6	21.1	48.7	0.0	0.0	0.0	x	Total	5.00	r	6795969.86	1974972.49	5.00
R5		R5	55.6	27.6	52.6	0.0	0.0	0.0	x	Total	5.00	r	6796278.73	1975777.07	5.00

## Point Source(s)

Name	M.	ID	Result. PWL			Lw / Li		Operating Time			Height (ft)	Coordinates				
			Day (dBA)	Evening (dBA)	Night (dBA)	Type	Value dB(A)	norm.	Day (min)	Special (min)		Night (min)	X (ft)	Y (ft)	Z (ft)	
AC1		AC1	88.9	88.9	88.9	Lw	88.9		675.00	0.00	270.00	4.00	r	6796778.59	1975704.85	4.00

## Line Source(s)

Name	M.	ID	Result. PWL			Result. PWL'			Lw / Li			Operating Time			Moving Pt. Src			Height (ft)
			Day (dBA)	Evening (dBA)	Night (dBA)	Day (dBA)	Evening (dBA)	Night (dBA)	Type	Value dB(A)	norm.	Day (min)	Special (min)	Night (min)	Number			

Name	ID	Height		Coordinates			
		Begin (ft)	End (ft)	x (ft)	y (ft)	z (ft)	Ground (ft)

## Area Source(s)

Name	M.	ID	Result. PWL			Result. PWL"			Lw / Li			Operating Time			Height	
			Day	Evening	Night	Day	Evening	Night	Type	Value	norm.	Day	Special	Night	(ft)	
			(dBA)	(dBA)	(dBA)	(dBA)	(dBA)	(dBA)			(dBA)	(min)	(min)	(min)		r
CONT1		CONT1	106.7	106.7	106.7	57.9	57.9	57.9	PWL-Pt	106.7					8	r

Name	ID	Height		Coordinates			
		Begin (ft)	End (ft)	x (ft)	y (ft)	z (ft)	Ground (ft)
CONT1	CONT1	8.00	r	6796755.45	1975710.74	8.00	0.00
				6796745.89	1976358.09	8.00	0.00
				6796988.94	1976359.82	8.00	0.00
				6797337.90	1976369.37	8.00	0.00
				6797381.30	1976352.01	8.00	0.00
				6797410.82	1976299.93	8.00	0.00
				6797426.44	1976244.37	8.00	0.00
				6797442.94	1976101.14	8.00	0.00
				6797439.46	1975909.30	8.00	0.00
				6797406.48	1975845.07	8.00	0.00
				6797422.10	1975752.18	8.00	0.00
				6797456.83	1975626.32	8.00	0.00
				6797446.41	1975518.68	8.00	0.00
				6797328.35	1975370.24	8.00	0.00
				6797179.92	1975207.91	8.00	0.00
				6797031.48	1975069.89	8.00	0.00
				6796857.87	1974926.66	8.00	0.00
				6796771.73	1974863.40	8.00	0.00
				6796754.06	1975681.22	8.00	0.00
				6796783.58	1975682.96	8.00	0.00
				6796782.71	1975710.95	8.00	0.00

### Barrier(s)

Name	Sel.	M.	ID	Absorption		Z-Ext.	Cantilever		Height		Coordinates				
				left	right		horz.	vert.	Begin (ft)	End (ft)	x (ft)	y (ft)	z (ft)	Ground (ft)	
						(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)

### Building(s)

Name	Sel.	M.	ID	RB	Residents	Absorption	Height	Coordinates			
								Begin (ft)	x (ft)	y (ft)	z (ft)
BUILDING			BUILDING0004	x	0	0.00	a	6796765.34	1975705.82	0.00	0.00
								6796777.13	1975706.13	0.00	0.00
								6796777.65	1975686.37	0.00	0.00
								6796765.65	1975686.06	0.00	0.00

### Ground Absorption(s)

Name	Sel.	M.	ID	G	Coordinates	
					x (ft)	y (ft)
					(ft)	(ft)

### Vertical Area Source(s)

Name	ID	Height		Coordinates			
		Begin (ft)	End (ft)	x (ft)	y (ft)	z (ft)	Ground (ft)

### Rail

Name	Sel.	M.	ID	Lw'		Train Class	Correct.	Vmax
				Day (dBA)	Night (dBA)			

### Sound Level Spectra

Name	ID	Type	Oktave Spectrum (dB)										Source			
			Weight.	31.5	63	125	250	500	1000	2000	4000	8000		A	lin	

### Roads

Name	Sel.	M.	ID	Lme			Count Data		exact Count Data			Speed Limit		SCS		Surface		Gradient (%)	Mult. Reflection			
				Day (dBA)	Evening (dBA)	Night (dBA)	DTV	Str.class.	M			p (%)			Auto (mph)	Truck (mph)	Dist. (dB)		Dstro (dB)	Type (dB)	Drefl (ft)	Hbuild (ft)

### RoadsGeo

Name	Height		Coordinates				Dist (ft)	LSlope (%)
	Begin (ft)	End (ft)	x (ft)	y (ft)	z (ft)	Ground (ft)		